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COMPUTER AUTOMATED DESIGN OF SYSTEMS

Larry Paul Vines

# NAVAL POSTGRADUATE SCHOOL

## Monterey, California



# THESIS

Computer Automated Design of Systems

by

Larry Paul Vines

June 1976

Thesis Advisor:

George J. Thaler

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Computer Automated Design  
of  
Systems

by

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Lieutenant, United States Navy  
B.S.E.E., Purdue University, 1970

Submitted in partial fulfillment of the  
requirements for the degree of

MASTER OF SCIENCE IN ELECTRICAL ENGINEERING

from the  
NAVAL POSTGRADUATE SCHOOL  
June 1976

## ABSTRACT

An automated digital computer technique of control system design is presented. The emphasis is on compensator design but the method is applicable to the design of any system with free parameters. Signal representation and system response are in the time domain.

The inputs required from the engineer are the system configuration, the desired output response and the free parameters. A parameter minimization routine is then used to minimize a specific cost function and to set the free parameters. A graphical output of the desired response and actual system response is then produced for comparison by the engineer.



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## I. INTRODUCTION

The past two decades have been witness to an ever increasing use of the digital computer. Engineering usage and design are probably the most important justification for the large memory, high speed computers of today. Classes in computer application to engineering problems have become part of the established curricula at most universities. Numerous papers have appeared on the application of the computer to engineering problems [1] which until recently were unsolvable or at best required long, tedious procedures which gave only approximate solutions.

Control system engineering has relied increasingly on computer simulation of large scale systems to verify that design specifications have been met and to make modifications to a system even before producing a prototype. There are programs available to simulate virtually any electrical circuit, or control system, either in transfer function form or as a system of first order differential equations. Others draw the Bode, Nichols or Nyquist plots of open and closed loop systems. Some programs help design compensators which use an iterative method to achieve the desired frequency response [2] [3]. Researchers continue to better adapt the computer to engineering usage.

Cantalapiedra [4] has used an iterative method to find the optimum reduced order model for large order systems. MacNamara [5] went even further and used an iterative method to find the optimum compensation for an aircraft autopilot. It would appear that these techniques could be extended and applied to the direct simulation and design of control

system circuits in the time domain.

The intent of this thesis was to develop a user oriented program which could simulate a wide variety of control systems and determine the values of the gains, poles and zeros necessary to produce a desired response. A convenient means of data card input was to be provided to specify (1) the control system which was to be optimized and (2) the desired response. A locally available function minimization routine (ECXFLX) was to be used to optimize the simulated system's output.

To simulate the system which is to be optimized, transfer functions which are commonly encountered were reduced to first order linear differential equations. These equations were then programmed so that the transfer function blocks could be connected in an arbitrary fashion by data card input. Several common nonlinear transfer blocks were also provided. The program will simulate the system with the known parameters and then allow all unknown or adjustable parameters to be fixed by the computer optimization routine to achieve the desired response.

## II. PROGRAM DEVELOPMENT AND IMPLEMENTATION

### A. GENERAL

Any program which is to be of maximum benefit to the user must have a simple means of data input and an output which is easy to interpret and apply to the problem at hand. The input data should have a physical significance that does not lose its relevance through the programming of numerous equations. The program should be a readily usable tool and not a problem in itself. The intent of this thesis is to present such a program, Computer Automated Design of Systems (CADS), which is readily used for simulation with optimization of the output. Optimum in the sense that the output response of a given system configuration is as near the desired response as possible.

Most control system design starts with a proposed transfer function block schematic to achieve a desired time domain response. CADS has the common transfer functions built into the program and the input data can come directly from the proposed system schematic. The transfer blocks which are available for system simulation are presented in Table I. These blocks should be adequate, either separately or in various cascade combinations, to represent most control systems.



TYPE  
CF  
BLOCK

SYMBOL

EQUATION SOLVED

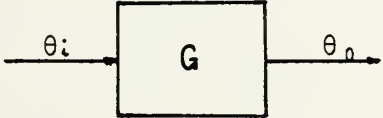
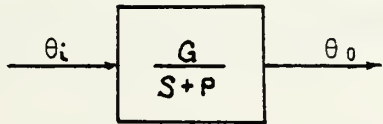
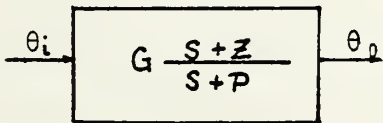
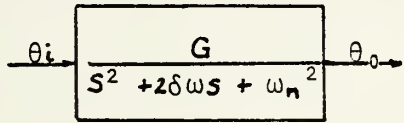
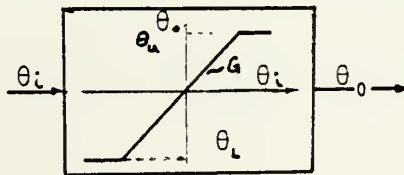
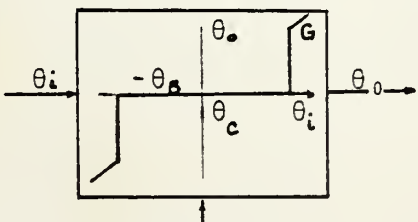
1		$\theta_o = G \theta_i$
2		$\dot{\theta}_o = -P \theta_o + G \theta_i$
3		$\dot{\theta}_o = -P \theta_o + G(\dot{\theta}_i + Z \dot{\theta}_i)$
4		$\ddot{\theta} = -2\delta\omega_n \dot{\theta}_o - \omega_n^2 \theta_o + G\theta$
5		$\theta_o = G \theta_i \quad \theta_l \leq G \theta_o \leq \theta_u$ $\theta_o = \theta_u \quad \theta_u < G \theta_i$ $\theta_o = \theta_l \quad G \theta_i < \theta_l$
6		$\theta_o = 0 \quad  \theta_c  < \theta_\beta$ $\theta_o = G \theta_i \quad  \theta_c  \geq \theta_\beta$

TABLE I Program Transfer Function Blocks

To use the program the engineer must know the system configuration in transfer block form and the desired second order output response. If other than a second order response is desired, this may be easily specified but requires some knowledge of how to input the desired response. CAIS will take the transfer block system, connect it, compare the given system response to the desired response and set any free parameters to achieve the closest match possible of the system output to the desired response.

Figure 1 is representative of the type of system the program can simulate and optimize. In figure 1, the parameters of the numbered transfer function blocks are known or fixed by equipment limitations. Transfer blocks X, Y, and Z contain variable parameters which must be selected by the program to make the system output reproduce a desired output function as closely as possible.

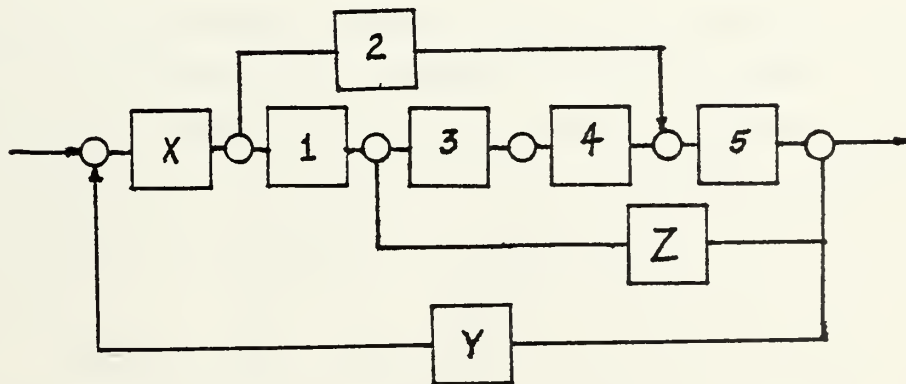


FIGURE 1 Typical System to be Optimized

## E. MAIN PROGRAM

The MAIN program was developed to control the selection of the subfunctions used in the optimization process and to compute the desired response of the systems which were to be optimized. A second order step response is calculated from equation (I) as the desired response and stored in the array XDATA.

$$\theta_o = \frac{G}{s^2 + 2 \delta \omega_n s + \omega_n^2} u(t) \quad (I)$$

The MAIN is essentially a bookkeeping routine which controls the program execution. The subfunction operations it controls are defined in the following sections.

## C. PLANT

The common simulation routines LISA, DSL, ECAP, CSMP and INTEG were investigated in an attempt to adapt them to the general problem specified above. These programs required either the input of the system's state variable equations, Laplace transform equations or the node-transfer function pair for each system simulated. These programs are useful for simulation if all of a system's parameters have been specified. However, each simulation is problem specific and these techniques are not readily integrated with other subfunction programs. A simulation subprogram which was capable of accepting data card input to simulate a wide variety of control systems and of working with other existing subprograms had to be developed.

Subfunction PLANT was developed to simulate the systems which were to be optimized. It provides the versatility necessary to simulate numerous system configurations and is capable of working with a minimization routine to optimize the variable parameters. The program reads the transfer function block connections from data cards. This data is then used to automatically set up the system equations in state variable format. These state variable equations are solved as first order, ordinary differential equations by the Runge-Kutta-Gill fourth order method. The programming was done in Fortran IV and all calculations are in double precision. The capability of connecting the transfer function blocks in any configuration (feed forward, feedback, etc.) is possible with this program. Simulation flexibility is provided by having each block within the system capable of accepting an external forcing function.

### 1. Block Data Card

Several possible ways of inputting the data necessary to simulate arbitrary system configurations were investigated. A means of defining a system configuration directly from a block diagram schematic was chosen as the most preferable method. Using this approach, each data card was designed to be directly related to a transfer function of the system. This resulted in having direct access to the transfer function parameters for optimization.

To simulate the system, a data card is prepared for each transfer block in the schematic diagram. The data card contains a field of numbers which specify the block number, the type of transfer function contained within the block, the input node and the output node to which the block is connected and the values of any parameters associated with the transfer function. The general format of the data

cards used to input the system configuration is shown below.

1	11	20	40	60	(Column Number)
---	----	----	----	----	-----------------

ELKCCD=EEVV	G	P	Z
-------------	---	---	---

Where:

CC = Position number of the block

D = Type of block (number)

EE = Input node number

VV = Output node number

G, P, and Z are parameters of the transfer function.

## 2. Block Connections

The number of transfer blocks in the system and the data cards associated with each of the blocks are read upon initial entry into the simulation routine. The program then connects the transfer function blocks in the proper order by comparing the input node number of a block to the output node number of every other block. Whenever these two numbers are equal, the blocks are known to be connected and a flag is set equal to 1.0. The flags are then used to identify the input drives to each block.

## 3. Drives

The input quantity to each block is called the DRIVE. The program was designed to allow for multiple inputs to the system being simulated. This flexibility was achieved by making the input to each block equal to the sum of the outputs of all blocks connected to the input node plus any external forcing function (DRVIN) feeding the transfer block. The input DRIVE to a block is determined as shown in equation (II).



$$\text{DRIVE}(i) = \sum \text{THA}(j) * \text{FLAG}(j,i) + \text{DRVIN}(i) \quad (\text{II})$$

THA(j) is the output of block j. FLAG(j,i) is 1.0 if block j is connected to block i and zero if it is not connected. DRVIN(i) is any external forcing function specified by the user which drives block i. DRVINS must be inserted in subroutine FLANT as Fortran IV statements. The standard program has DRVIN(1) = 1.0 specified as a unit step input to the system. Problem III-E in the section Investigation of Program Performance demonstrates how multiple, time varying inputs are to be inserted in the program.

#### 4. Standard Transfer Function Blocks

The transfer function blocks available for system simulation are shown in Table I. These blocks were selected because of their common usage in the modeling process. They were also found to be adequate either separately or in various cascade combinations to represent most control systems.

The transfer function equations for each type of block were written in state variable format and stored in an array named THA. The program reads a number from a block's data card which specifies the type of transfer function associated with the block. The system equations are then solved sequentially by selecting the type of equation associated with block number one, solving for its output and then sequencing to block number two, etc. The integral equations are solved by a modified RKL fourth order method in the subfunction routines. Three integration routines were necessary to store the intermediate results obtained for those equations involving a double integration. The four subfunctions, RKLDE2, RKLDE3, CCPLX and RKLDE4 are called by FLANT. RKLDE2 is used for the integration of a

type two block. RKLDE3 is used for integration of a type three block and to store intermediate quantities for subfunction CCPLX. CCPLX calls RKLDE3 and RKLDE4 for integration of a type four block.

No provision has been made for the input of initial conditions or the integrators. Therefore, the integrations must start at time equal zero. The user must specify the step size to be used for integration (DT) and the problem run time (TF). To conserve computer time DT should be made as large as possible.  $DT = TF/1000$  is suggested as appropriate in most cases. Equally important is that TF be as small as possible. Use of the program has shown that letting TF be greater than the transient response time of the system is rarely justified. For preliminary analysis TF was kept to only slightly longer than the time of the first undershoot for second order dominant systems. Because of the complexity of subroutine PLANT a flow chart of PLANT has been included as Appendix B.

## 5. Parameters to be Optimized

The parameters of the system which are to be optimized by the minimization routine EOXPX must be specified in PLANT. The minimization routine returns the trial values of the variable parameters to PLANT in an array labeled 'C'. Regular Fortran IV statements equate the variable parameters to the values in this array. If a pole-zero pair were to be optimized, the following statements would be inserted in PLANT:  $P(i) = C(1)$  and  $Z(i) = C(2)$ . The location for the preceding statements is clearly indicated in the program listing for PLANT.



#### D. DESIRED RESPONSE (XDATA)

The criteria against which the system response will be compared will vary according to the application of the system. Since most design work on control systems is done on the basis of second order dominance, the program was written to provide a second order step response with adjustable  $\delta$ ,  $\omega_n$  and gain as the basic criteria against which the simulated system will be compared. The desired  $\delta$ ,  $\omega_n$  and gain are read in as input data. The step response is then computed in the main program by subfunction RKLDEC and stored in the array called XDATA. Any other time domain response may be specified by the user by removing the second order step response equations and replacing them with the equations of the desired response. An example is provided by problem III-E in Investigation of Program Performance. If the program is being used for simulation only and no data curve is desired, setting the input variable LEAP = 1 will cause the program to bypass the computation of the standard second order data equation.

#### E. COST FUNCTION (PERFORMANCE INDEX, PI)

The achieved system response is compared with the desired response and the difference is the error. The program searches for the parameter settings which will minimize this error. The cost function may be specified by the user to weight the system outputs as desired in subfunction FE. The default cost function of the program is

the integral error squared.  $J = \int_a^{TF} (\text{Err})^2 dt$ . An example of a weighted cost function is presented in Section III.

## F. MINIMIZATION ROUTINE

### 1. General

The free parameters are optimized to reduce the cost function by the complex method of M. J. Box.[6] Box's constrained optimization method has been programmed at the Naval Postgraduate School by R. R. Hilleary as a subroutine called ECXPLX. This subroutine will find the minimum of an arbitrary function (cost function) subject to arbitrary explicit constraints and for implicit constraints. Explicit constraints are defined as upper and lower bounds on the free parameters. Implicit constraints may be arbitrary functions of the free parameters (e.g.  $P_1 P_2 < 178$ ).

Two function subprograms are used to evaluate the objective function and implicit constraints, FE and KE respectively. The method BOXPLX uses to search for the values of the free parameters which minimize the cost function is explained in the computer program listing.

### 2. Explicit/Implicit Constraints and Start Points

ECXPLX searches a feasibility region (n-dimensional space, where  $n$  = number of free parameters) defined by upper and lower bounds on the free parameters for a minimum cost function. The smaller the region defined by these boundaries, the more rapidly the program will converge to the optimum parameter settings. Good engineering judgement will be necessary to keep the feasibility region as small as

possible. The boundaries of the search region are read from data cards by the main program as the upper bound (XU) and the lower bound (XL) for each free parameter.

Implicit constraints may be any arbitrary function of the free parameter desired. If an implicit constraint such as the product of a pole-zero pair must be less than some number is to be evaluated, it must be supplied by the user to the subfunction KE. No implicit constraints were used in this thesis.

The starting values of the free parameters (XS) are read in by the MAIN from data cards. A good choice of starting values will dramatically reduce the time required for optimization. A preliminary root locus or Bode plot method of estimating the best values of the free variables should be accomplished whenever possible.

#### G. GRAPHICAL OUTPUT

Two subroutines were written to provide for the graphical output of the desired response and the best system response achieved by the optimization process. The user may select, by data card input, either subroutine PPLT which provides a high speed printer plot or subroutine PIC which provides a calcomp graph. Every fifth integration point stored in the arrays XDATA and THAOUT is plotted. Subroutines PFIT and PIC call the subroutines PLOTP and DRAW respectively. PLOTP and DRAW are standard plotting routines at the NPS computer facility and are not a part of the simulation program. Figure 2 diagrams the information flow and data input to the program.

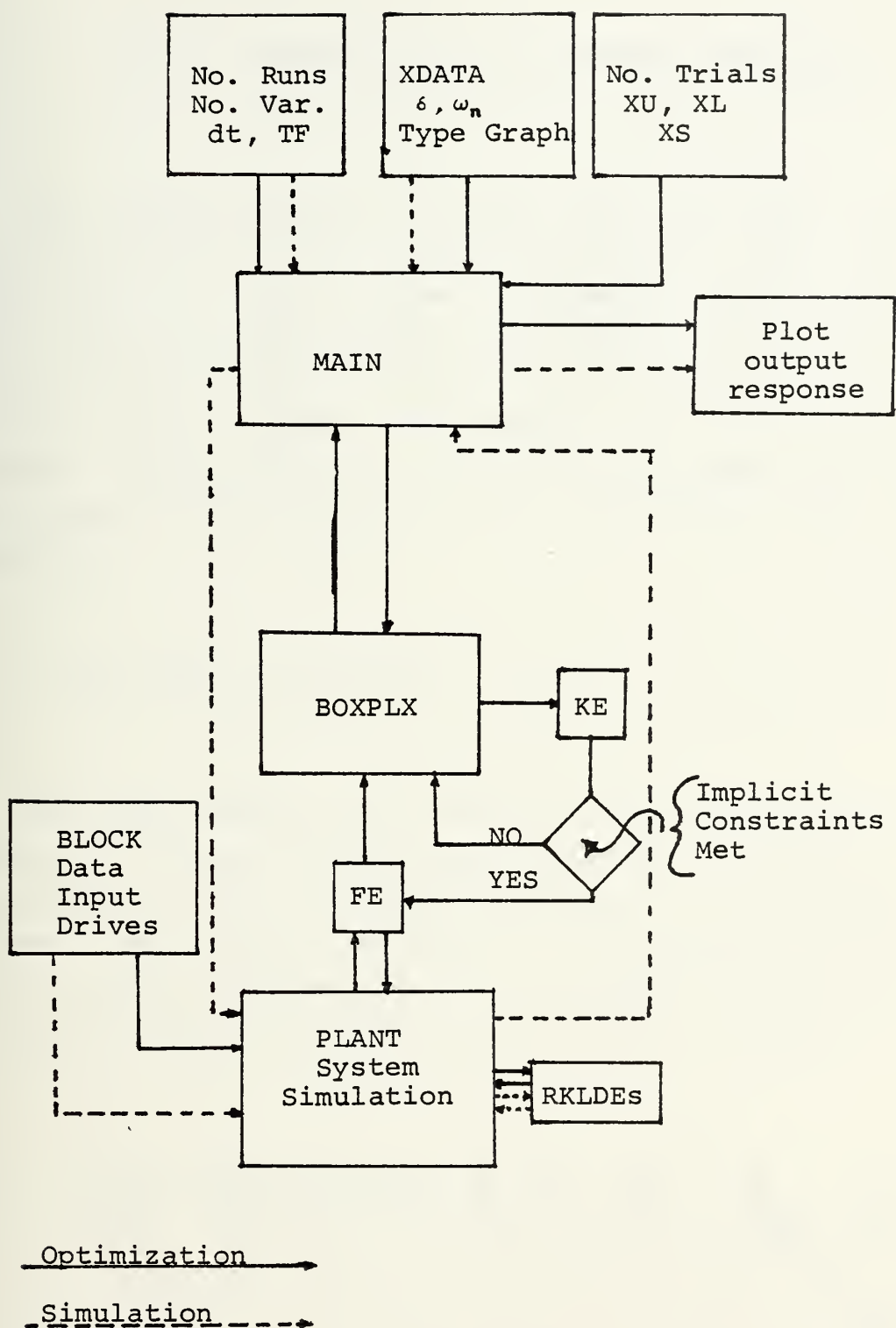


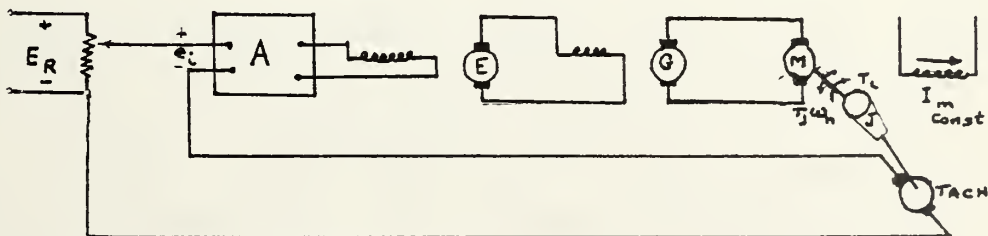
FIGURE 2 CADs Program Flow Chart

### III. INVESTIGATION OF PROGRAM PERFORMANCE

The example problems presented below were used to aid in the development of the optimization program. The order of difficulty of the problems progresses from a simple text book single variable, single input system to a multivariable operational servo drive system which has multiple inputs and discrete level feedback. An example of how a schematic diagram representation of a system is prepared for input to the program is presented prior to considering the example problems.

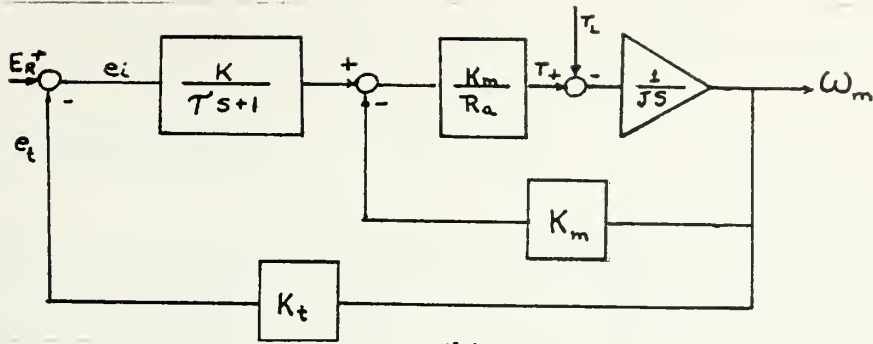
#### A. DATA INPUT, AN EXAMPLE

The Ward-Leonard drive system [7] shown schematically in Figure 3 (a) has two variable parameters. The gain of the amplifier and the tachometer feedback are available to adjust the system's response. To simulate the system a block diagram representation of the system is drawn as shown in Figure 3 (c) using the transfer blocks from Table I.

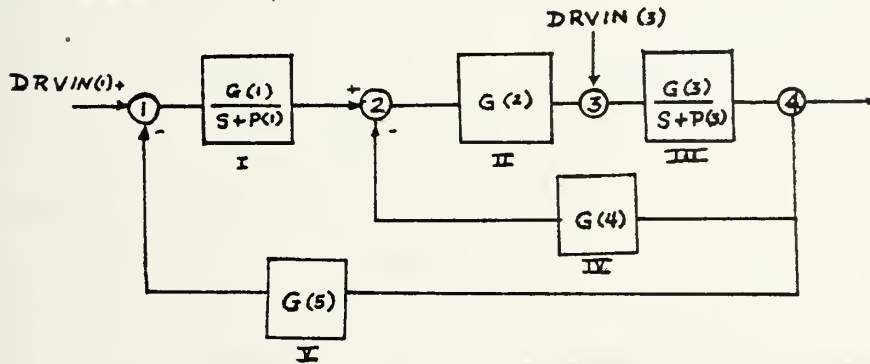


(a)





(b)



(c)

FIGURE 3 Ward - Leonard Speed Control System  
Using Feedback. (A) Schematic Diagram  
(B) Block Diagram (C) Block Diagram  
Using CADS Blocks.

Where

$$\begin{aligned} G(1) &= K/\tau & P(1) &= 1/\tau \\ G(2) &= K_m/R_a \\ G(3) &= 1/J & P(3) &= 0 \\ G(4) &= -K_m \\ G(5) &= -K_t \\ \text{DRVIN}(1) &= E_r \\ \text{DRVIN}(3) &= -T_L \end{aligned}$$

The nodes of the block diagram are then numbered sequentially 1,2,...,n. The blocks between the nodes are also numbered sequentially 1,2,...,N as shown in Figure 3 (c). Data cards (N) are then prepared for each block which specify the block number, type of block, the input node, the output node, and the parameters contained within the block. In Figure 3 (c), for example, block 1 is



a type two transfer block connected between nodes 1 and 2. The data card input for this block would be

BIK012=0102

$K/\tau$

$1/\tau$

The program reads the data card input and connects the blocks by setting a FLAG = 1. whenever the input node number to a block is the same as the output node number of any other block. The input to a transfer block is then determined to be the sum of the outputs of all blocks connected to the input node plus any external forcing function driving the input node. The program has a unit step specified for DRVIN (1). If this is the only input to the system, no action is necessary on the part of the user. If other than a unit step input to the system is desired or if there are other external forcing functions such as DRVIN (3), they must be specified and placed within the body of the subfunction PLANT as Fortran IV statements. For the example shown in Figure 3 (c), a card with the equation

$$\text{DRVIN}(3) = f(T_L)$$

would have to be inserted preceding the drive equations. An example of how multiple, time varying drives are specified is given in section III. E.

When optimizing a system, some of the input quantities will be unknown or variables. These variables must also be assigned within subroutine PLANT. To optimize the variables  $K_1$  and  $K_t$  of Figure 3 the following two statements would be inserted in PLANT:

$$G(1) = C(1)$$

$$G(5) = C(2)$$

where C(1) and C(2) are the variables which will be optimized by subroutine BOXPLX.

## E. TACHOMETER FEEDBACK

The first optimization problem attempted was one which had an exact solution that can be found by algebraic methods. An instrument servo [8] with unity feedback and forward transfer function

$$G(S) = \frac{1000}{S(S+10)} \quad (\text{III})$$

was to be compensated with tachometer feedback as shown in Figure 4. The only specification for the system's performance of this single variable, second order system was the simple requirement that the closed loop roots have a  $\delta = 0.7$ .

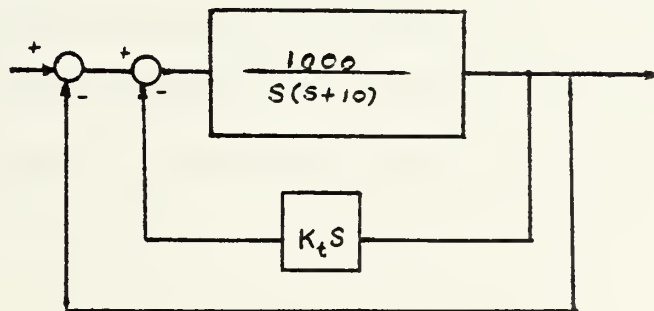


FIGURE 4 Tachometer Compensated System

The system shown in Figure 4 was redrawn as Figure 5 in order to achieve the tachometer feedback. The characteristic equation of the system shown in figure 5 is

$$S^2 + (10 + 10^3 K_t) S + 10^3 = 0 \quad (\text{IV})$$

The required  $K_t = 0.0343$  may be calculated from equation IV.

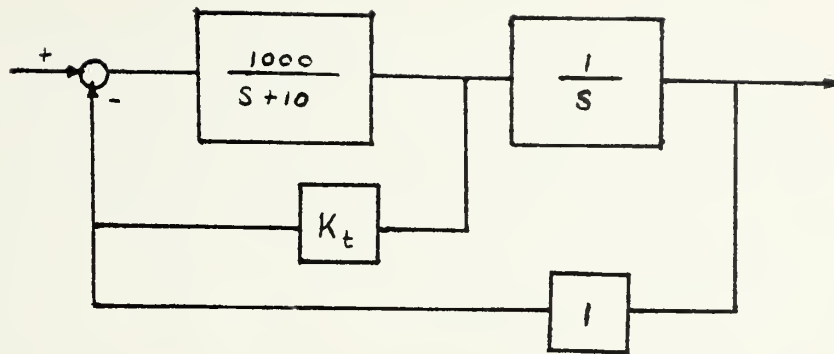


FIGURE 5 CADS Block Diagram of Tachometer System

CADS was programmed to optimize the system with the variable,  $K_t$ , specified to be between the limits  $0.01 < K_t < 1.0$ . The desired response was specified to be the standard second order step response for  $\delta = 0.7$ ,  $\omega_n = 1000$ . CADS determined the optimum value for  $K_t$  to be  $K_t = 0.0343$ . Figure 6 shows the system's step response and the desired response are virtually superimposed.

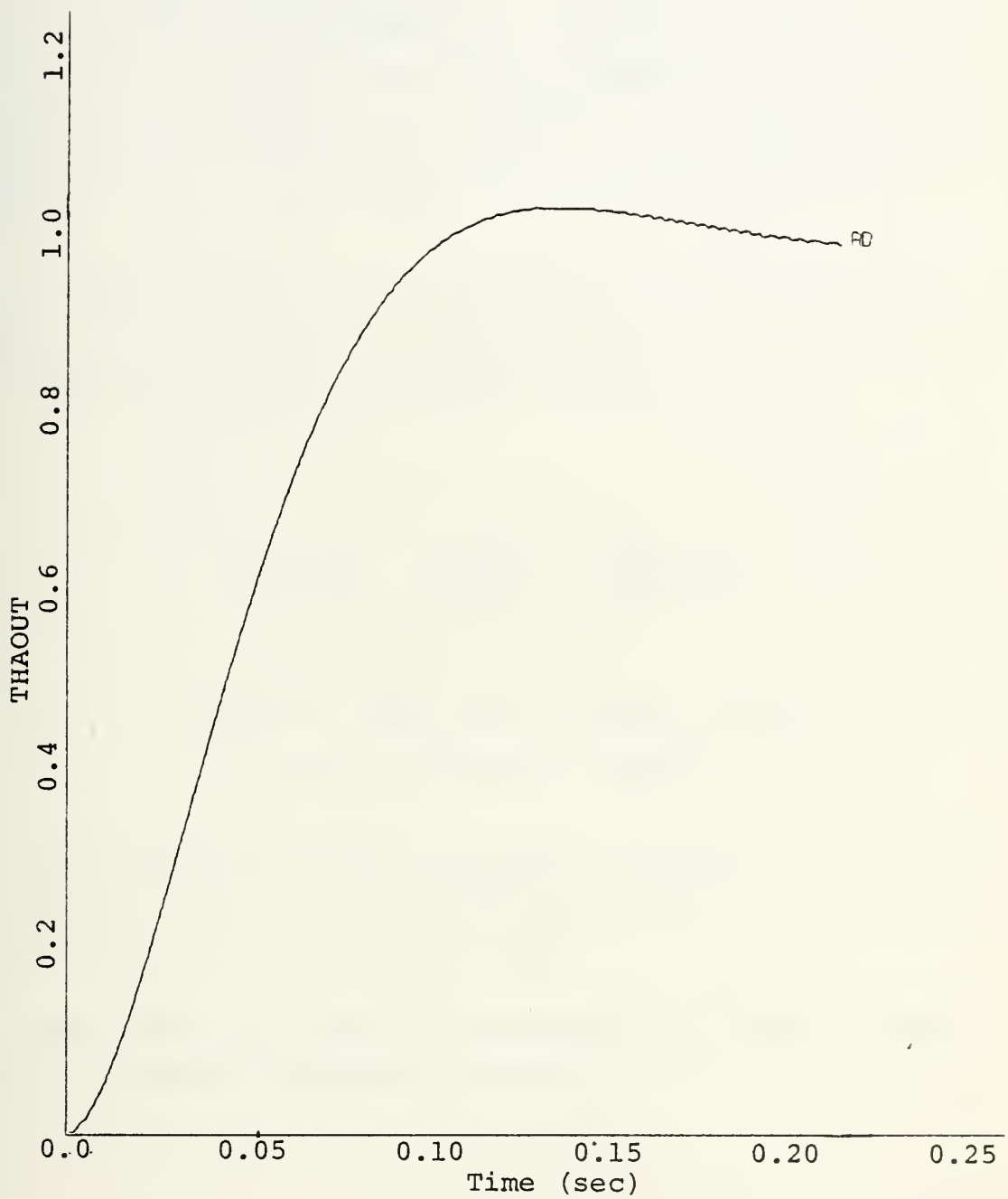


FIGURE 6 CADS Compensated Tachometer Feedback  
System Response

The type one system, in the preceding example, allowed derivative feedback from the forward path without requiring a block which was capable of differentiation. One may encounter a type zero system or a system which cannot be configured to provide derivative feedback from the forward path. The possibility of providing a pseudo derivative feedback using a type three block was investigated for these cases.

A type three block with  $Z = 0$  and  $G = P$  is shown in Figure 7. If the pole is placed far out on the real axis, this block approximates derivative feedback.

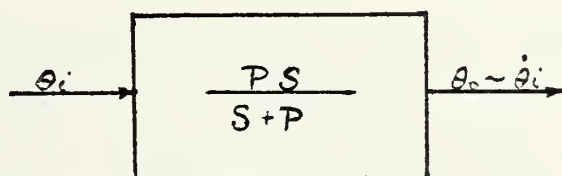


FIGURE 7 Type Three Block used for  
Pseudo Tachometer Feedback

The effect of using this pseudo tachometer feedback on the complex roots of the closed loop system is negligible. It does add a real root at  $P = -964$ .

The system of Figure 5 was redrawn as shown in Figure 8 using the pseudo tachometer feedback.

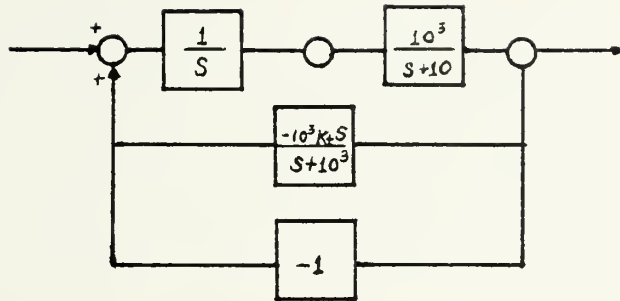


FIGURE 8 Pseudo Tachometer Feedback

The optimization program calculated  $K_t = 0.0352$  for the above configuration. This gave a  $\delta = 0.715$ .

The system response and the desired response are shown in figure 9. The two responses are again nearly superimposed. This method of providing derivative feedback has the disadvantage of adding an integration step to the problem solution with the concomitant increase in problem solution time.



FIGURE 9 Pseudo Tachometer Compensated System's Response



### C. CASCADE COMPENSATION

Having proven the feasibility of the program optimizing a single variable system where an exact solution was available, the next problem considered extending the problem scope to a third order plant with two variables. The unstable plant that was to be compensated is shown in Figure 10.

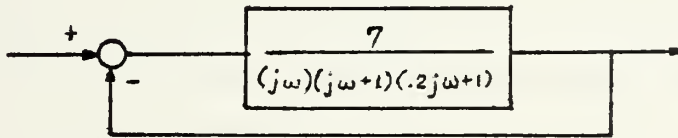


FIGURE 10 Third Order Plant to be Compensated

The plant was to be stabilized using a single section cascade compensator. The compensated plant was required to have  $M_{PW} < 2$ , without reducing the error coefficient. [8] The compensated system is shown in Figure 11. To keep the error coefficient constant, the compensator used was a simple lag network ( $\tau_1 < \tau_2$ ).

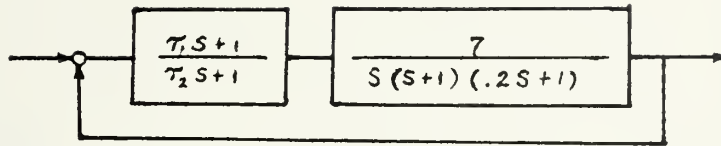


FIGURE 11 Lag Compensated System

A compensator which would meet the required specifications was calculated by conventional methods as a check on the program's performance. The Bode plot of the uncompensated and conventionally compensated system is shown in Figure 12. The values of  $\tau_1$  and  $\tau_2$  for Figure 11 which would meet the design requirements were determined to be  $\tau_1 = 10.$ ,  $\tau_2 = 100.$  The compensated system's response using these values for the compensator is shown in Figure 13.

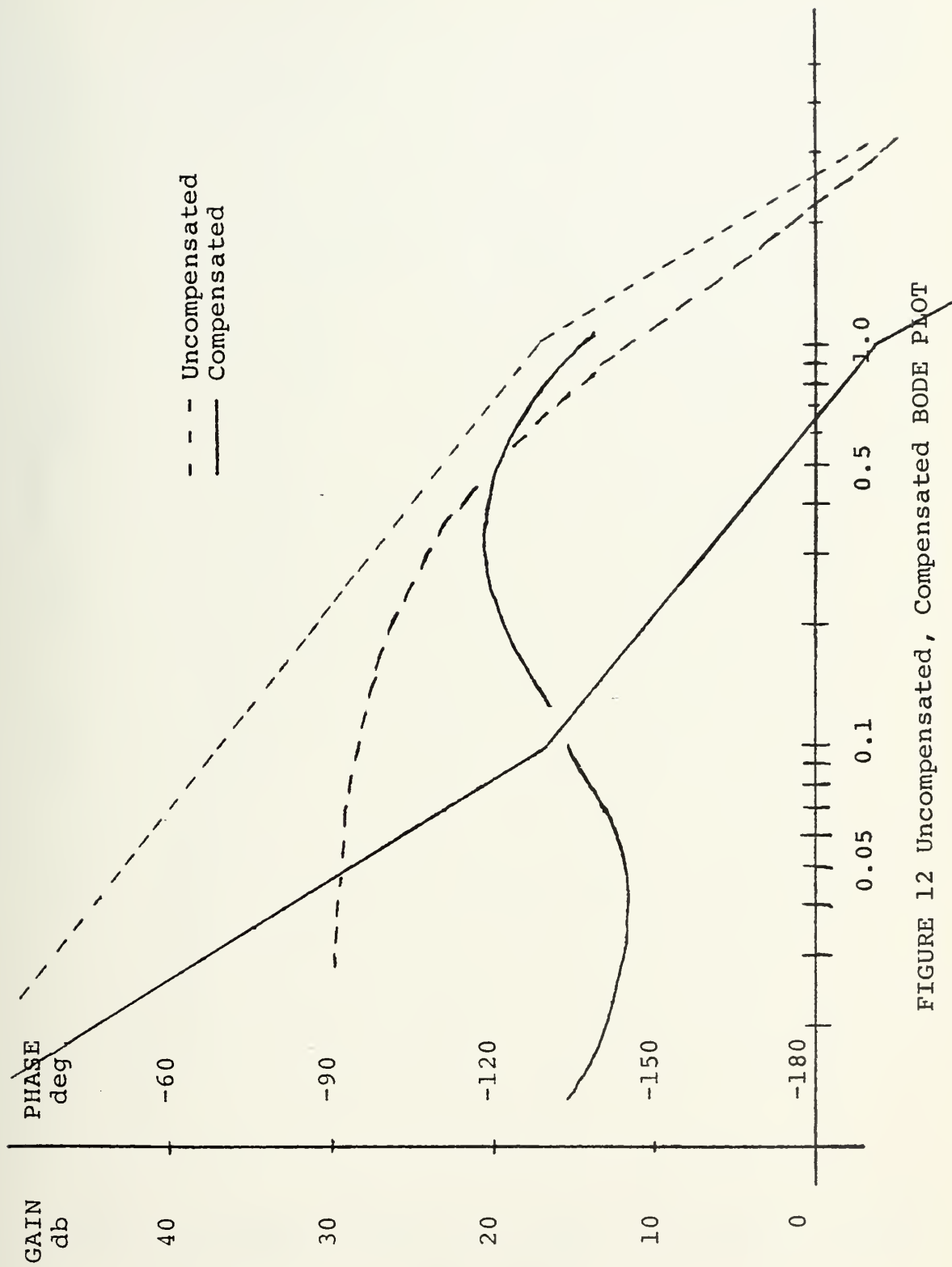


FIGURE 12 Uncompensated, Compensated BODE PLOT

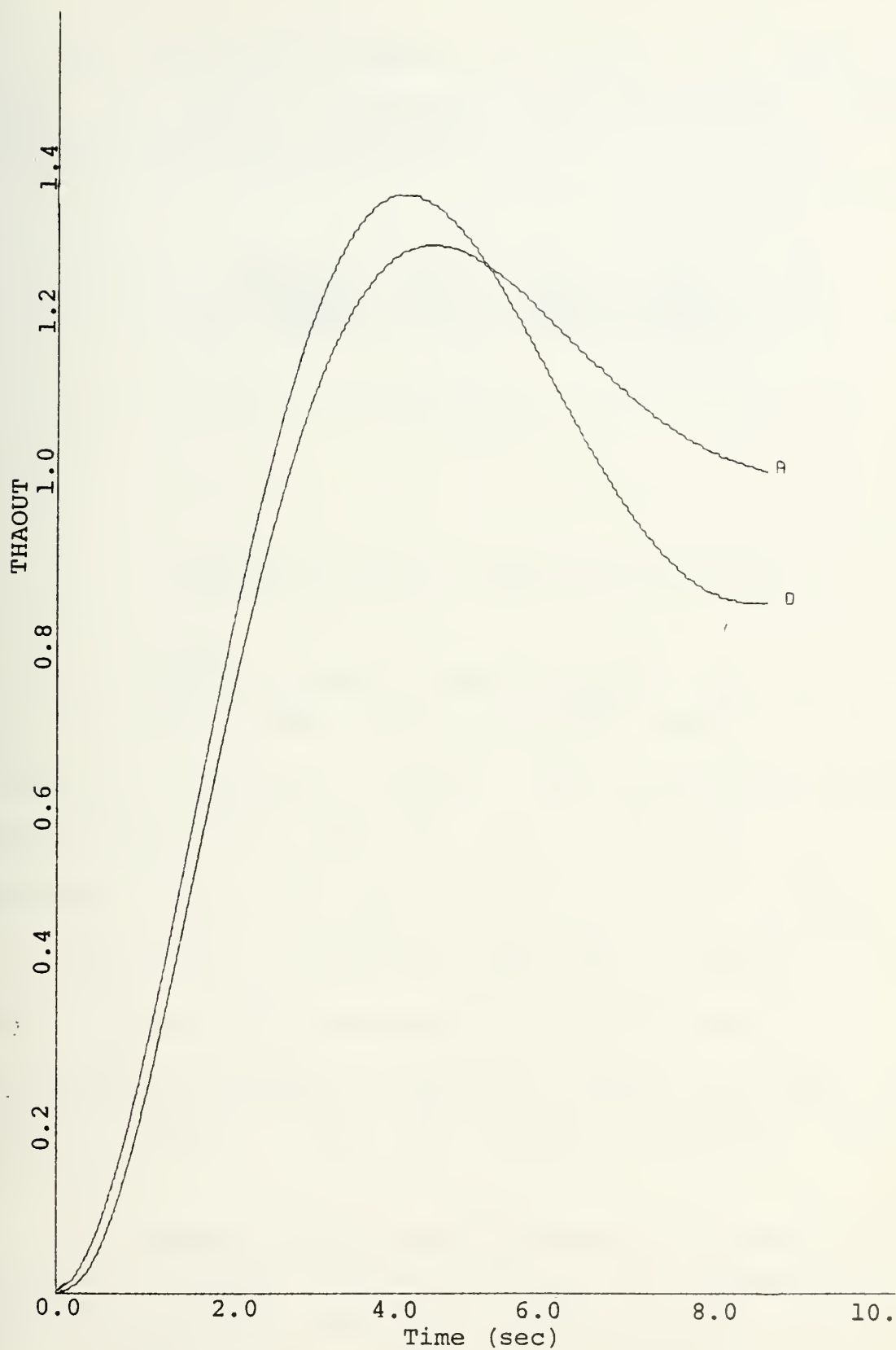


FIGURE 13 Conventionally Ccompensated System Respcnse

The compensated system was redrawn as shown in Figure 14 using the standard program transfer blocks available for system simulation.

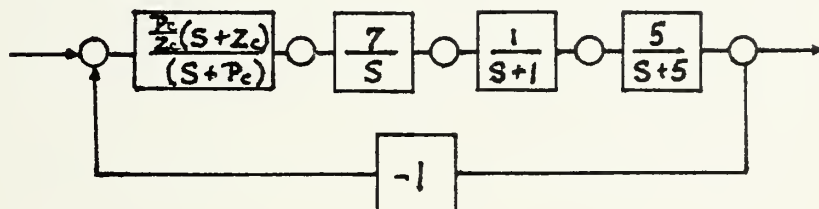


FIGURE 14 CADS Lag Compensated System

A standard second order response of  $\delta = .3$ ,  $W_n = 0.75$  was chosen as the desired response for the optimization program to match. The limits placed on the optimization program were  $.001 < P_c < .1$  and  $.01 < Z_c < 1$ . Arbitrary values to begin optimization were specified as  $P_{Co} = .01$  and  $Z_{Co} = .1$  in the logarithmic centers of the search zones. CADS determined  $\tau_1 = 8.078$  and  $\tau_2 = 67.47$  as the optimum parameter settings. Figure 15 shows the desired response and the program compensated system response.

The response of the system compensated by CADS is more nearly the desired response than is the conventionally compensated system. One should remember that the specified response is for a true second order system whereas, the compensated system is fourth order. Therefore, a perfect

match of desired versus actual responses could not be obtained.

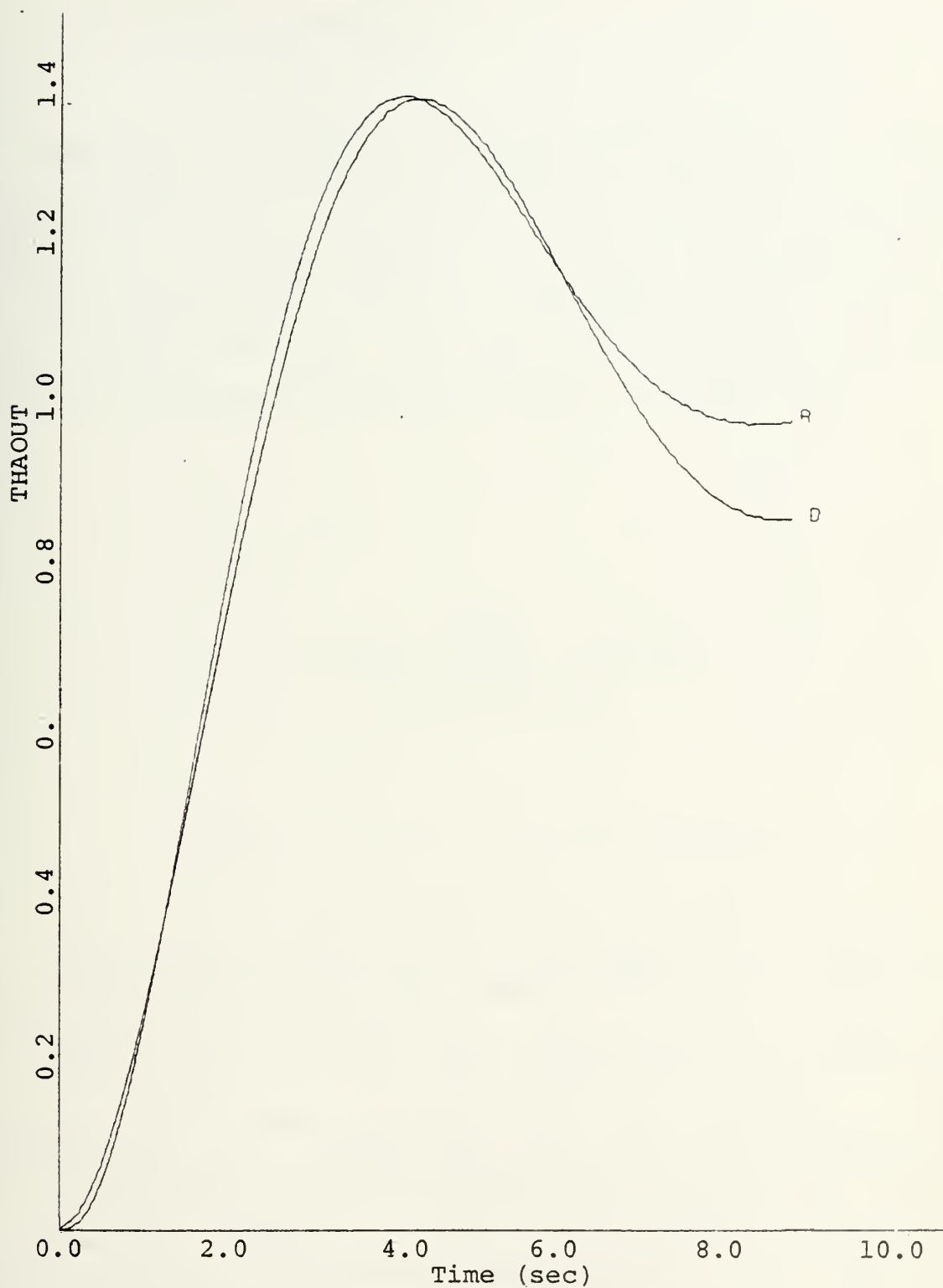


FIGURE 15 CADS Compensated System Response



## D. CASCADE LEAD COMPENSATION

The complexity of the next problem to be solved by CADS was extended to five free parameters. The plant shown in figure 16 was to be used to follow a unit amplitude sine-wave input of 200 rad/sec. The output amplitude was to be almost exactly the same as the input amplitude, and the output could not lag the input by more than  $10^\circ$ . Two sections of cascade compensation were to be used. [8]

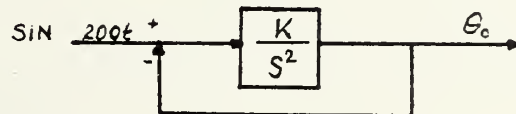


FIGURE 16 Plant for Lead Compensation

The specified requirements may be interpreted as an open loop gain  $> 15$  db and a phase angle  $\sim 90^\circ$  at  $\omega_n = 200$  from a Nichols plot. A cut and try solution on a Bode plot showed that a gain of  $3 \times 10^6$  and two phase lead compensators with a double zero at  $Z = 70$  and a double pole at  $P = 700$  will satisfy the closed loop magnitude and phase requirements. Figure 17 shows the system response and desired response obtained for these values. The magnitude of the compensated system's response is 93% of the desired response and lags by  $8.12^\circ$ .

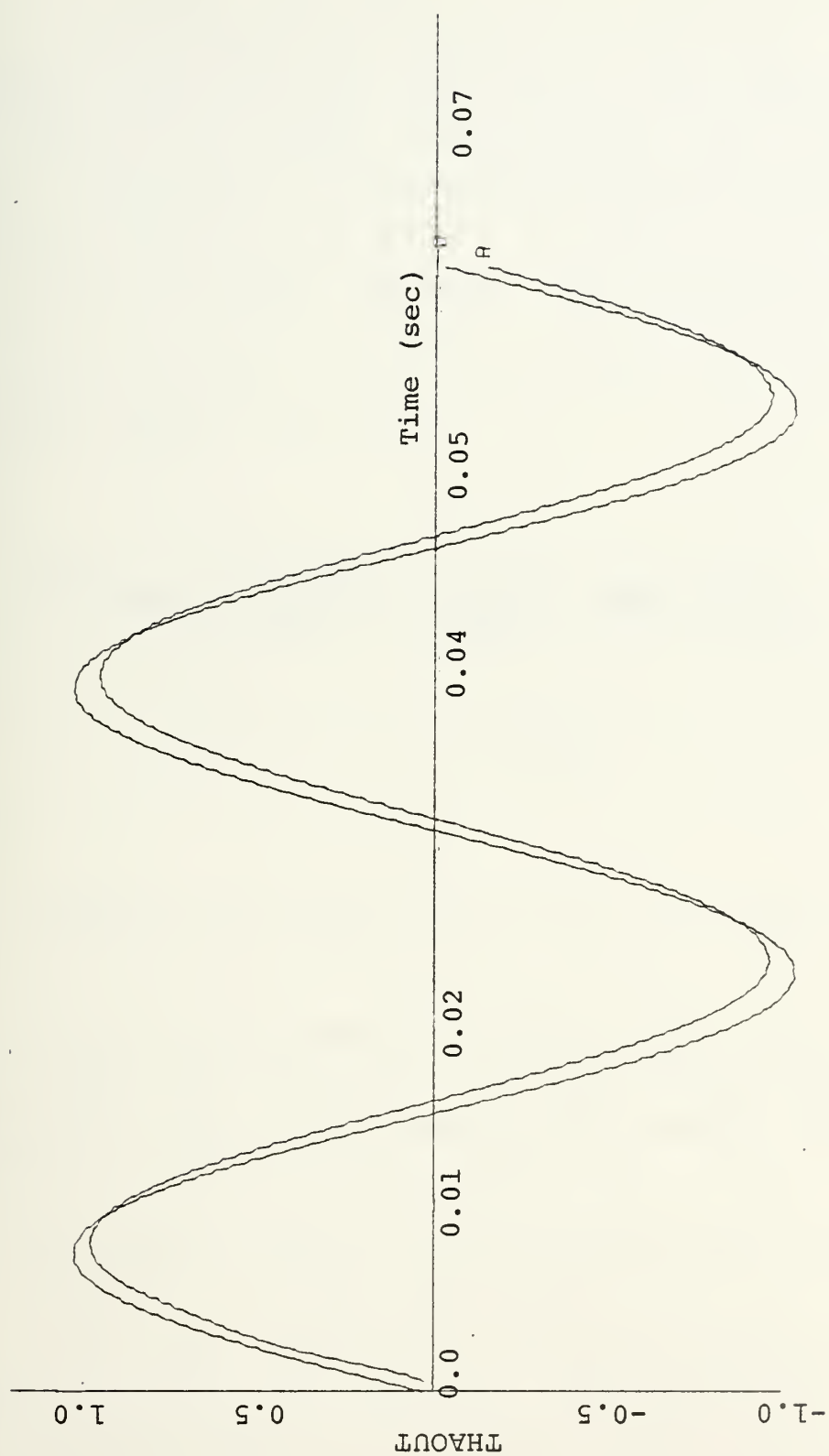


FIGURE 17 Conventional Lead Compensated System Response

The problem was then run on the optimization program with the block connections as shown in Figure 18. The free parameters were the poles and zeros of the compensators and the gain of the plant. The desired data curve of  $XDATA = \sin(200t)$  was generated from the standard second order step response by setting  $\delta = 0$ ,  $\omega_n = 200$  and using  $X(2)$  as the desired response. The initial search zone limits were specified as  $600 < P_i < 800$ ,  $60 < Z_i < 80$ ,  $2.8 \times 10^6 < G(3) < 3.2 \times 10^6$ .

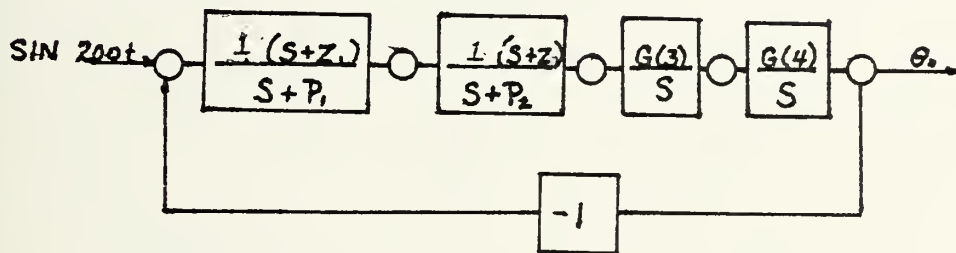


FIGURE 18 CADS Block Diagram for Lead Compensation

The optimization program solution went to the lower limits for both poles and the upper limits for both the zeros and the gain. The limits of the search zones were relaxed to  $500 < P_i < 600$ ,  $80 < Z_i < 90$  and  $3.2 \times 10^6 < G(3) < 3.4 \times 10^6$ . The program again placed the free variables on the limits of  $P_i = 500$ ,  $Z_i = 90$ , and  $G(3) = 3.4 \times 10^6$ . The system and desired response for these values is shown in Figure 19. The system magnitude and phase are much closer to the desired output response than the response of the conventionally designed compensator.

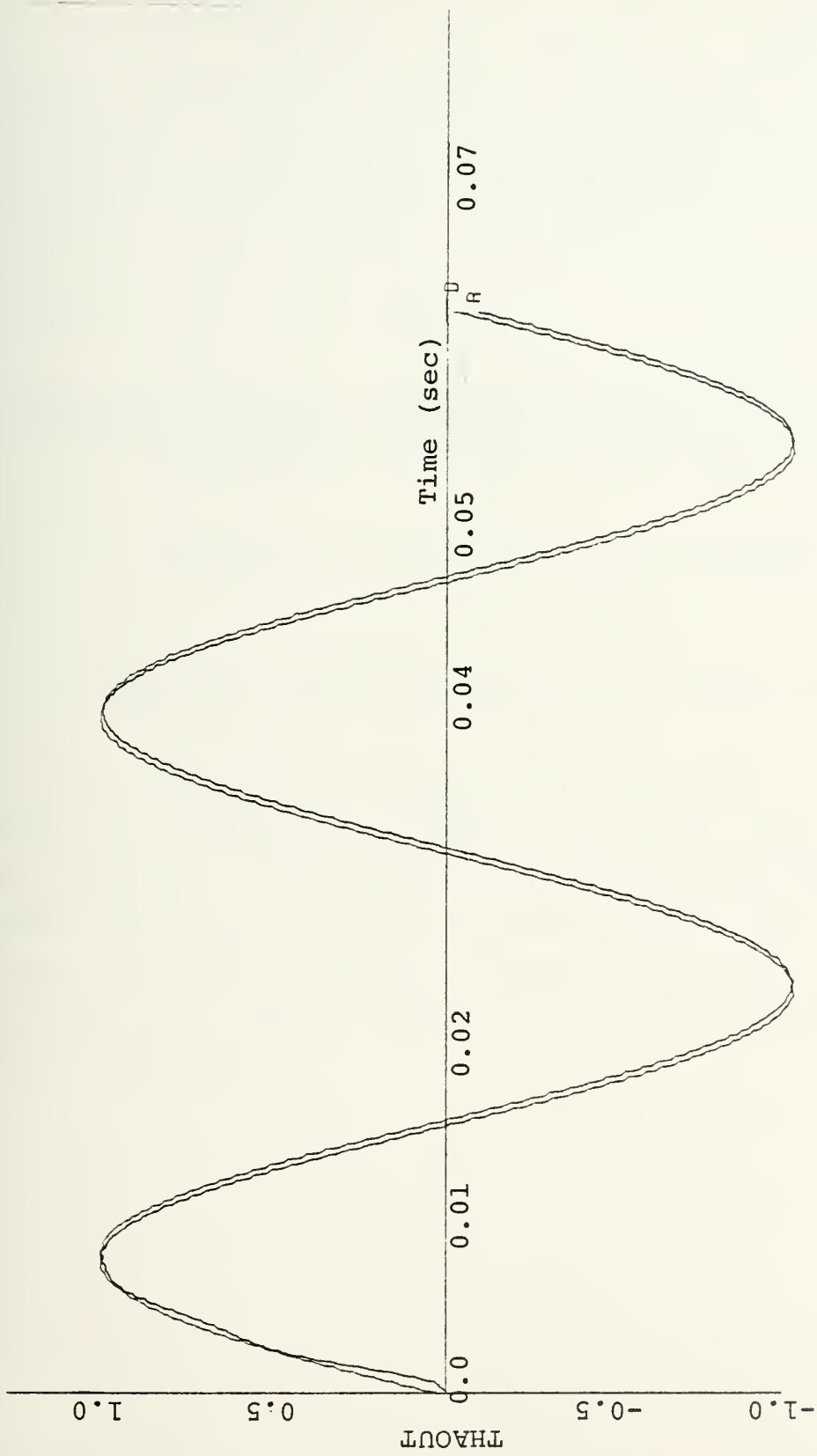


FIGURE 19 CADS Lead Compensated System Response

The phase difference is only  $4.33^\circ$ . Continued relaxation of the boundaries produced the compensated system shown in Figure 20. Figure 21 is a plot of the system's response for these values. The system's response is improved in that it lags the input by only  $3.46^\circ$  and the magnitude is essentially the same as the input magnitude.

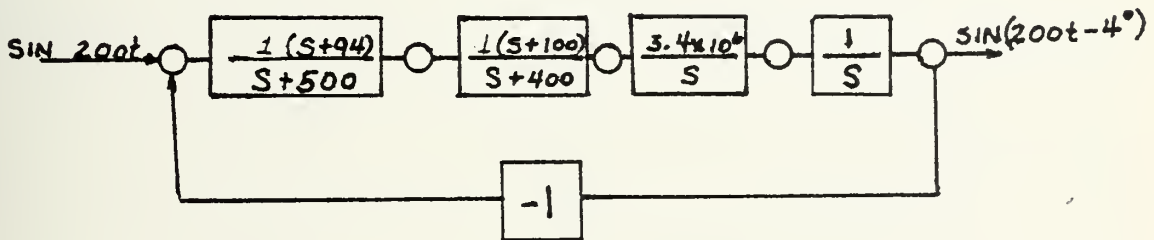


FIGURE 20 CADS Compensated System Block Diagram

The optimization program was activated at  $T = 0$  although the problem specifications were for the steady state response. The problem was rerun with the optimization process started after the transient had died out. The same values for the optimum compensator were obtained. Apparently the small initial transient did not effect the problem solution.

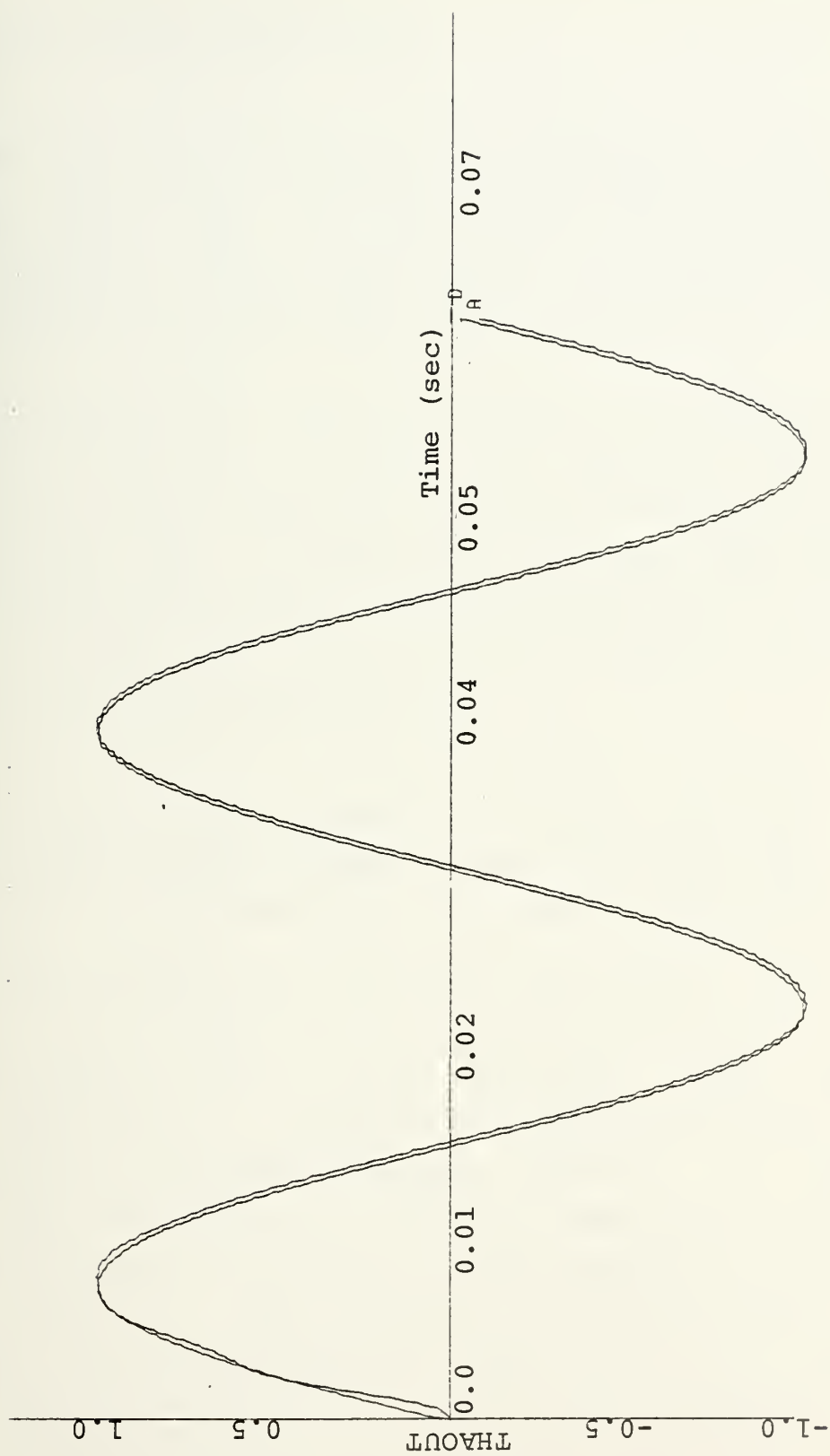


FIGURE 21 CADS Relaxed Boundary System Response

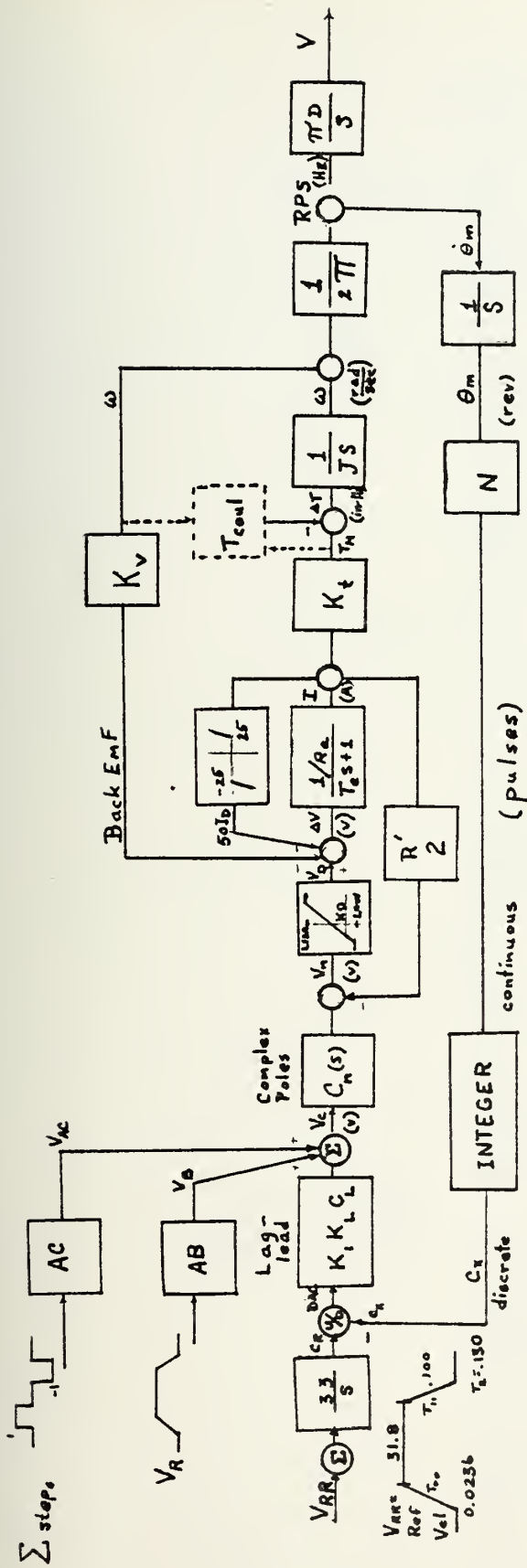
## E. SERVO SYSTEM COMPENSATION

The foregoing examples of the simulation - optimization program were simple examples which could obviously be quickly solved with the standard cut and try methods. A more complex and challenging example of program usage is presented by the system shown in Figure 22.

The system is an operational servo drive mechanism with multiple inputs and discrete level feedback. This highly nonlinear system's output was to follow the input as closely as possible and in steady state ( $t \geq 75\text{ms}$ ) there was to be very little noise ripple. The free parameters of the system are the poles and zeros of the compensator,  $C_L$ , and the poles of the noise suppressor  $C_n$ .

To simulate and optimize the system it was redrawn using the available program blocks as shown in Figure 23. During simulation it was found that the current limiter for  $I_D$  was not needed because  $|I_D| < 25\text{ A}$  and the limiter was removed to decrease program run time. The desired response (XDATA) was written as a set of three equations. These equations were then used to replace the second order step response equations in the standard program. DRVIN(1), (4) and (5) were also written as a set of equations and placed in subroutine FLANT. The discrete level feedback to block two was achieved by making  $\text{DRVIN}(2) = \text{INTEGER}(\text{THA}(12))$ . These changes to the main program and FLANT were all that were necessary to simulate this system. The implementation of these changes to the program is shown on pages 80 and 81.





$$AC = \frac{A J R_a}{K_i K_D}$$

$$AB = \frac{K_v}{r K_D}$$

$$A = \frac{1}{2} \frac{V_p^2}{X_a}$$

$$X_a = \frac{3}{8} \text{ in.}$$

$$V_p = 31.8 \text{ (in./sec)}$$

$$V_R = A \sum \text{Ramps}$$

$$C_L(s) = \frac{(1+s/50)^2}{(1+s/20)(1+s/500)}$$

$$C_n(s) = \frac{\omega_n^2}{s^2 + 2\delta\omega_n s + \omega_n^2}$$

$$\delta = 0.5, \omega_n = 1300$$

$$T_c = 2.425 \text{ (lb.)}$$

$$T_e = \frac{L}{R_a}$$

$$K_i = 1.6$$

$$K_L = 3.48$$

$$K_D = 2$$

$$L_{im} = 20$$

$$LOW = -4$$

$$N = 52$$

$$K_v = 0.086$$

$$K_T = 0.765 \left( \frac{\text{in. lb.}}{\text{A}} \right)$$

$$R_a = 0.5 \text{ (}\Omega\text{)}$$

$$L = 50 (\mu H)$$

$$J = 0.0016 \text{ (in. lb. sec}^2\text{)}$$

$$r = \frac{(\pi D)/8}{2\pi}$$

$$D = 4.016 \text{ in.}$$

$$r_o = \frac{\pi D}{8}$$

FIGURE 22 Servo Drive Mechanism, Original Compensation

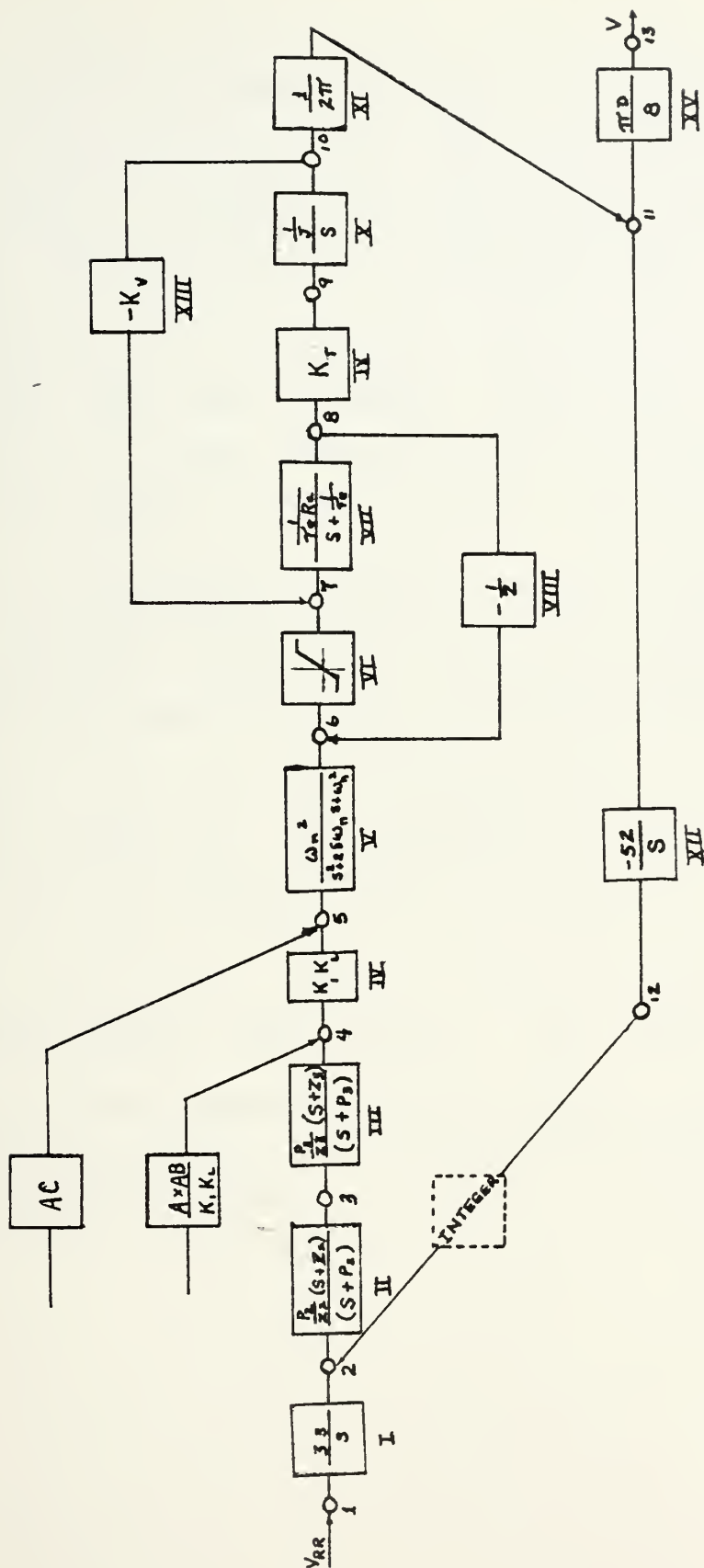


FIGURE 23 CADS Diagram of Servo Drive Mechanism

The system optimization was initially broken into two parts. This was to reduce the number of variables that were to be optimized per run and to obtain near optimum starting values for the free parameters. The above steps were taken in an effort to decrease the computer time required for a solution. The first run was to optimize the compensator,  $C_I$ , independent of the noise suppressor. The second optimization run was to select values for the noise suppressor,  $C_N$ . The rationale behind this separation was that the two circuits perform different functions and should therefore be initially separable in their effects on the system. The final optimization run was to be made with all free parameters available to the program for optimization. The search zone centered on the values found above.

Figure 24 shows the response for the system as originally compensated. The optimization run to set the values for  $C_I$  resulted in  $Z_1 = 43.5$ ,  $P_1 = 21.0$ ,  $Z_2 = 47.5$ ,  $P_2 = 592.0$ . Figure 25 shows the simulation of the system using these values. The initial velocity overshoot has been reduced and the average velocity after the transient appears more equally distributed above and below the desired velocity.

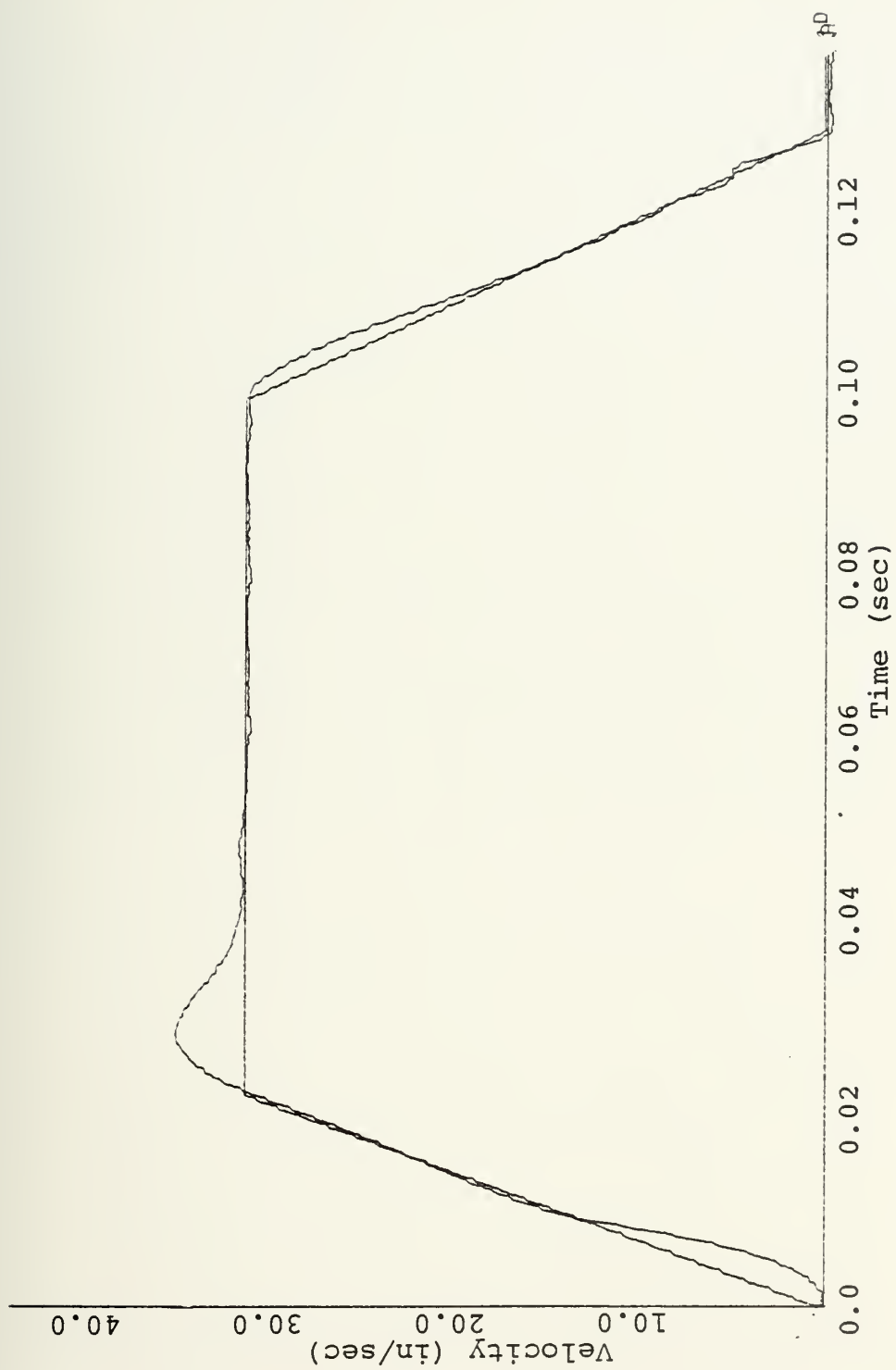


FIGURE 24 Original Servo System Response

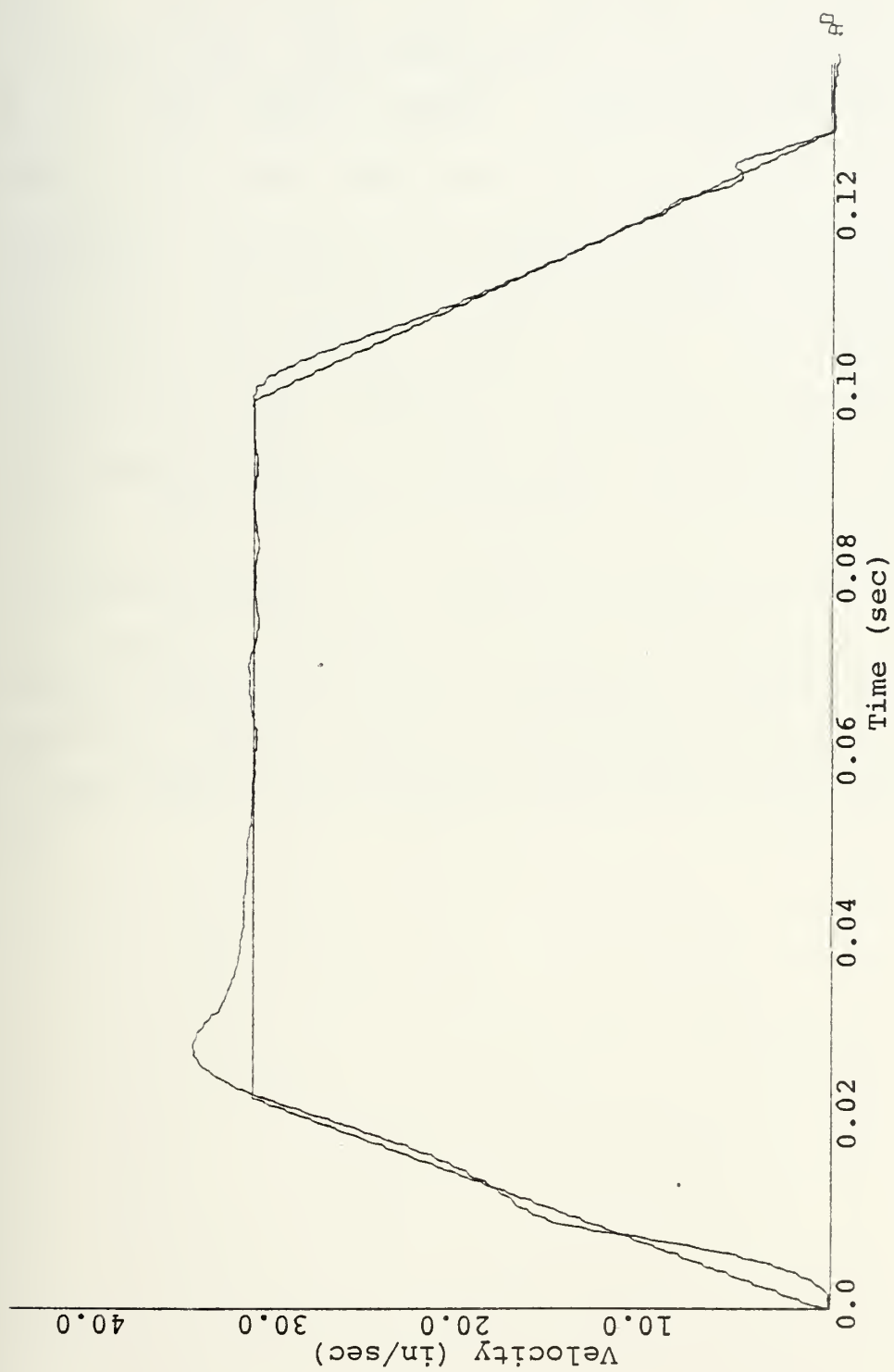


FIGURE 25 CADs Compensated  $C_L$  System Response

The initial optimization run for setting the values of the noise suppressor used the same cost function which had been used for all previous optimization runs  $J = \int \text{Err}^2 dt$ . This resulted in  $\delta = 0.2$  (lower bound), and  $W_n = 1500$  (upper bound). Figure 26 shows the result of using this cost function was to further decrease the overshoot. However, it allowed larger switching or noise transients as a result of weighting large transient errors more than the lesser noise jitter. To overcome this problem, the cost function was changed to  $J = \int |\text{Err}| * t * dt$ . This was to weight the steady state errors more heavily than the transient errors. Using this cost function the values set by the optimization program were  $\delta = .2$  and  $W_n = 1430$ . The damping factor,  $\delta$ , was again placed on the lower limit. The initial overshoot was still improved over the original system's response but the switching transients were not improved over the previous optimization trial. The results of the simulation run using these values is shown in Figure 27.

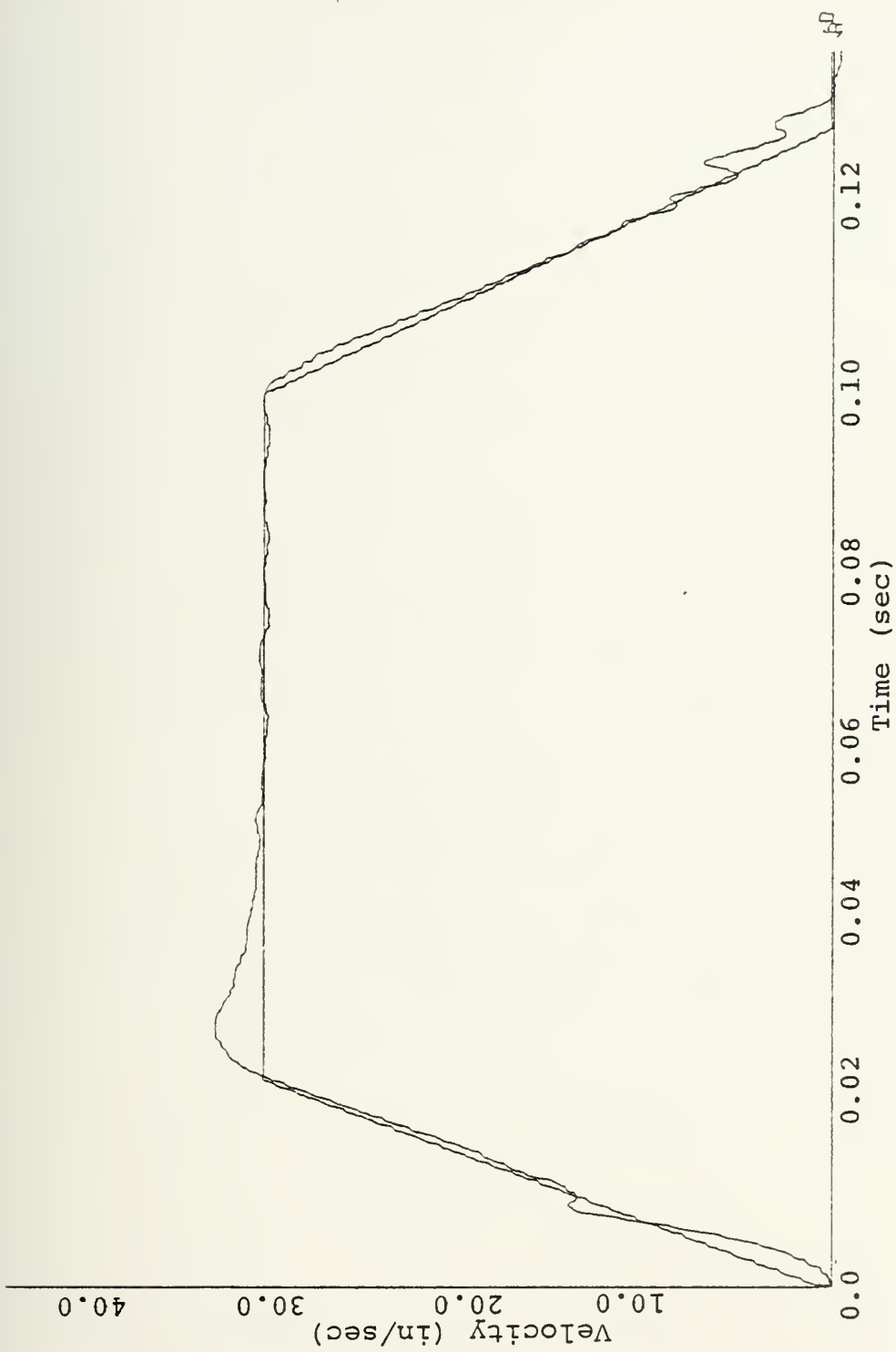


FIGURE 26 CADs Compensated C-1 System Response<sub>N</sub>



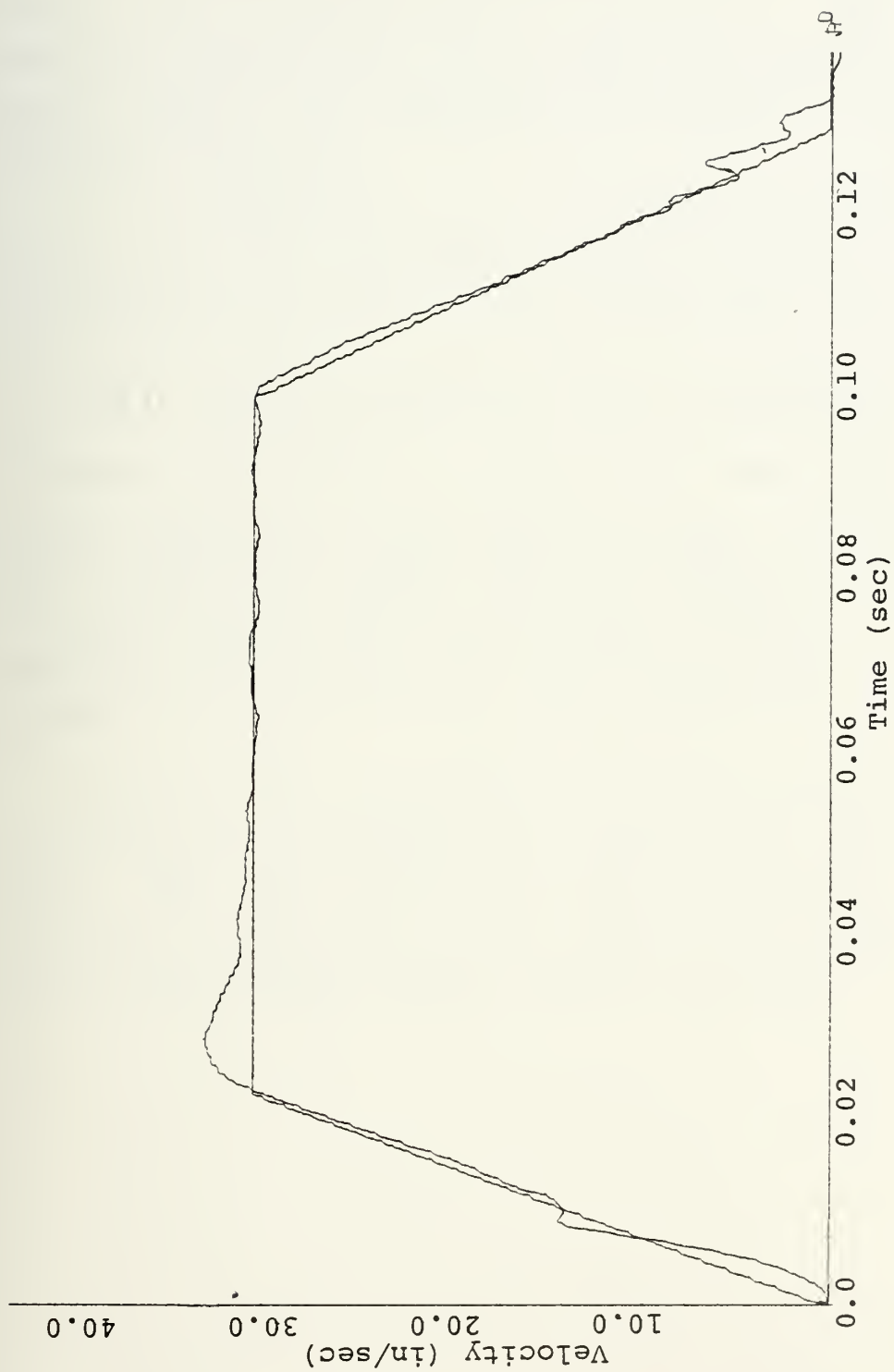


FIGURE 27 CADS Compensated C<sub>N</sub>-2 System Response

A final optimization run was made with all six variables free. The performance index was changed to the weighted cost function shown in equation V. The weighting factor was computed to equally weight the start up transient and the steady state responses in an effort to reduce the switching transients.

$$J = \int |Err| dt \quad 0.0 \leq T \leq 0.045$$

$$J = \int 4.14 * |Err| dt \quad 0.045 < t \leq TF \quad (V)$$

The optimum compensator values established by CADS were  $P_2 = 27.1$ ,  $Z_2 = 52.5$ ,  $P_3 = 521.$ ,  $Z_3 = 48.1$ ,  $\delta = 0.32$  and  $W_n = 1268$ . Figure 28 shows the fully compensated system's response. The initial overshoot has been reduced and the average velocity in steady state is closer to the desired value than the original system's response. However, the transient error on shut off is still present. Table II. summarizes the results of the optimization of the servo system.

The CPU time required for the optimization process was not decreased by splitting the problem into two separate parts. The time required for each optimization run on the individual compensators was the same as the time required to optimize the complete system with six variables.

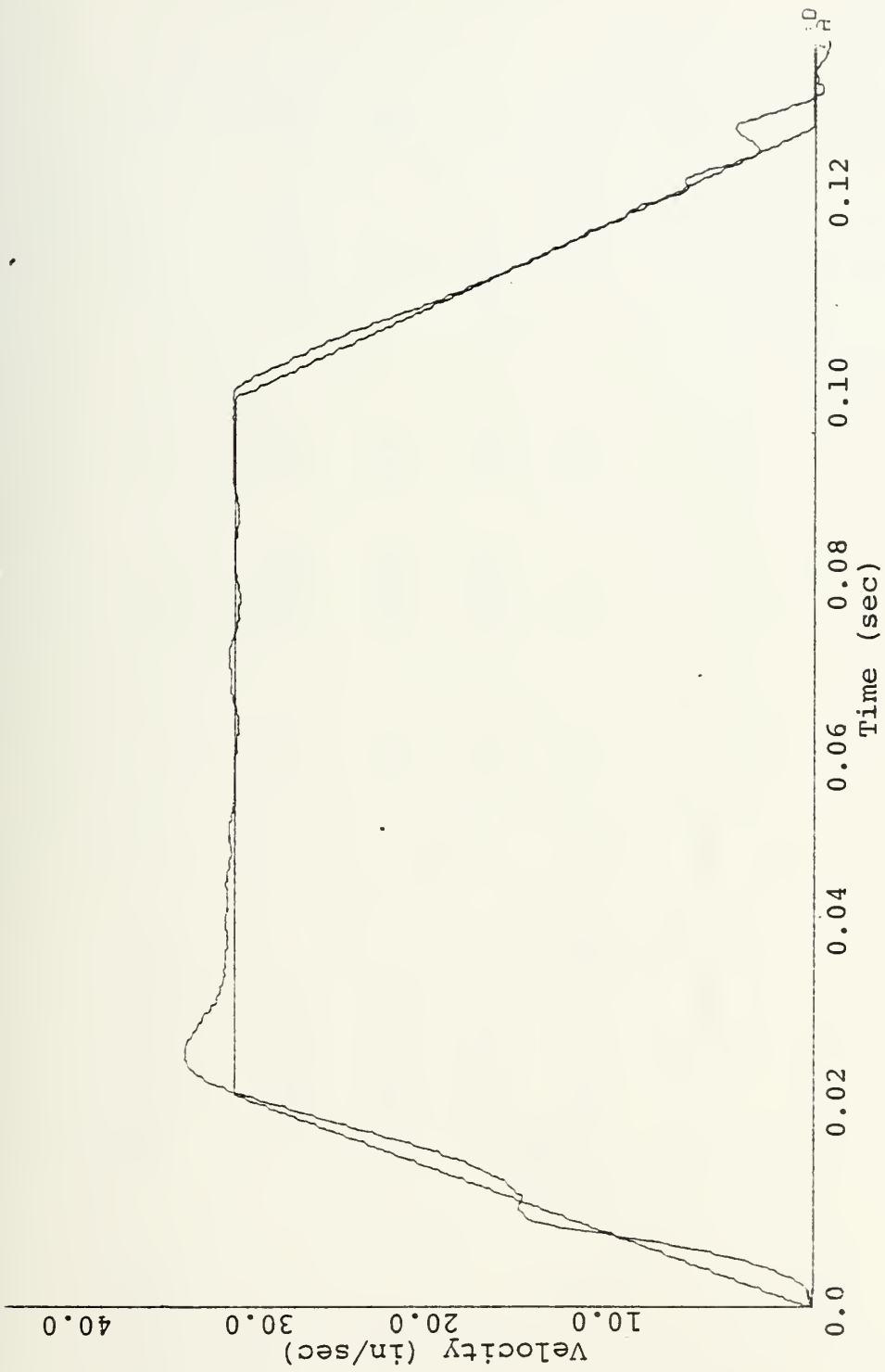


FIGURE 28 CALS Optimized System Response

Compensator	Ccost Function	P <sub>2</sub>	Z <sub>2</sub>	P <sub>3</sub>	Z <sub>3</sub>	δ	W <sub>n</sub>
Original		20.	50.	500.	50.	0.5	1300
C <sub>I</sub>	$\int \text{Err}^2 dt$	21.	43.45	592	47.47	0.5	1300
C <sub>N</sub>	$\int \text{Err}^2 dt$	21.	43.45	592	47.47	0.2	1500.
C <sub>N</sub>	$\int_{0.045}^{\infty}  \text{Err}  * t dt$	21.	43.45	592	47.47	0.2	1430.
C <sub>I</sub> , C <sub>N</sub>	$\int_{0.045}^{\infty}  \text{Err}  dt + 4.14 \int_{0.13}^{\infty}  \text{Err}  dt$	27.1	52.5	521.	48.	0.32	1268.

TABLE II Summary of Servo Drive Optimization

This problem has presented an excellent example of the necessity to carefully select the cost function which will measure the system's performance. Defining a performance index which will weight the more objectionable characteristics of a system's response so that they are eliminated or reduced becomes difficult as the system's complexity increases. The performance index,  $J = \int (\text{Err})^2 dt$ , was not adequate in its treatment of the noise and switching transients for the above problem. The other performance indexes used were also marginal in their effects upon parameter optimization. Although the cost function was reduced to a mathematically correct minimum, the system's performance was not the best that could be achieved. The system's performance was only optimum due to the definition of the cost function. The system was simulated using the compensator values determined from the last optimization run with the exception of  $\delta$  which was increased to  $\delta = 0.5$ . This simulation was made based upon engineering judgment of the effects of varying  $\delta$ . Figure 29 shows that this change in the damping factor produced a system response which was nearer the desired response than any of the previous runs.

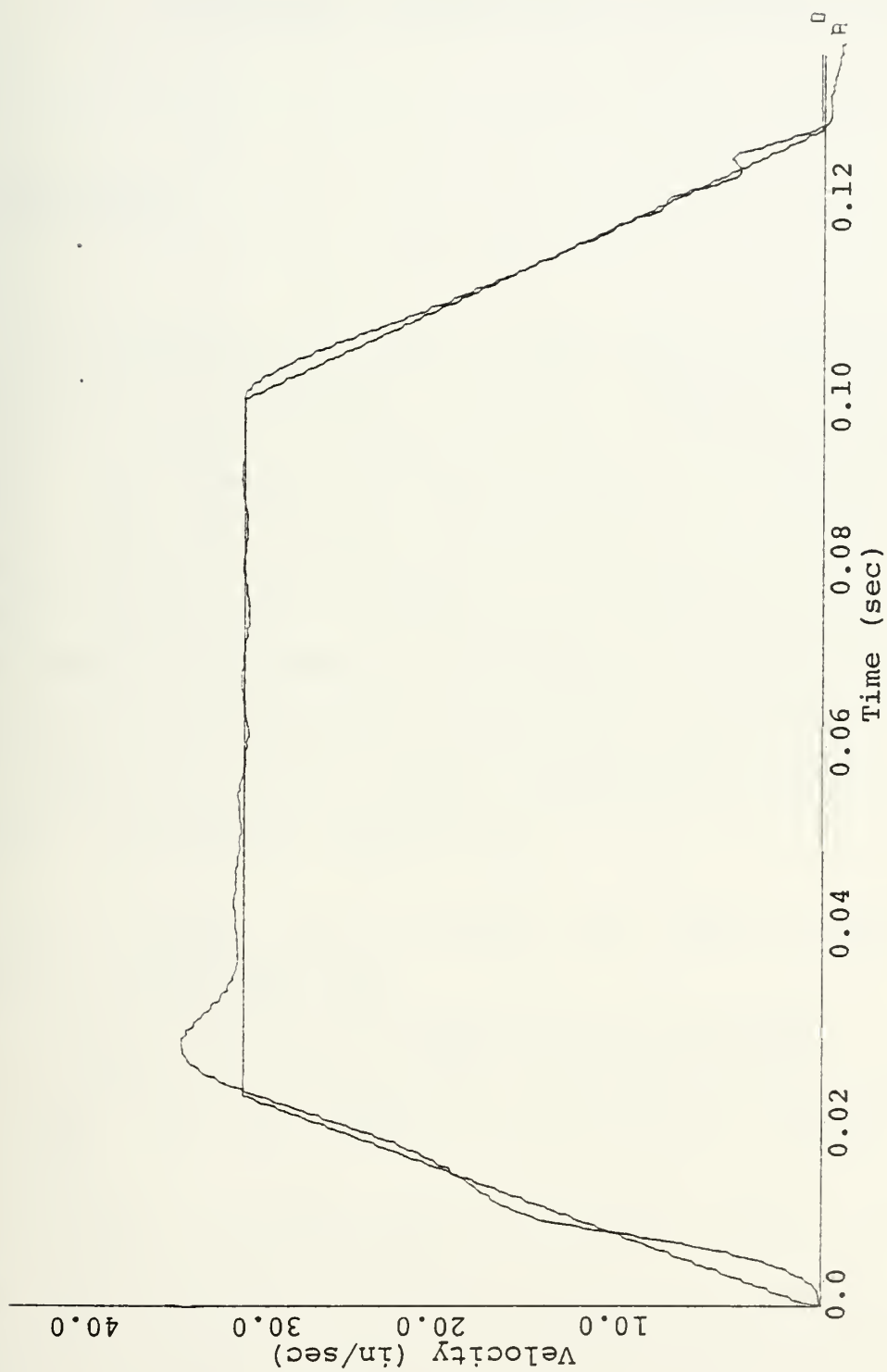


FIGURE 29 Servo System Response, CADS values with  $\delta = 0.5$

#### IV. DISCUSSION, CONCLUSIONS AND RECOMMENDATIONS

##### A. DISCUSSION

The objective of this thesis was to investigate the feasibility of developing a computer program which would optimize a variety of control systems' responses in the time domain. The program developed during the investigation proves that time domain optimization of control system responses is not only feasible but desirable due to the readily interpretable results of the optimization process. CAES requires approximately 200K bytes of computer core when the high speed printer plot is used for graphical display of the output and 230K when outputting calcomp graphs. These core requirements are a maximum and could be reduced by more careful, professional programming.

The computer time required for CAES to arrive at a solution is dependent upon

- (1) the order of the system being simulated,
- (2) the area of the search zone determined by the upper and lower bounds on the variable parameters and
- (3) the nearness of the starting guess to the optimum parameter values.

Every trial value of a parameter selected by FOXPLX requires a complete simulation of the system in order to evaluate the system's response and compare it with the desired response. The program run time is therefore,  $T_{RUN} =$  the number of trials  $\times$  system simulation time. A high order system may



require twenty seconds of CPU time for simulation. If 300 trials are required to determine the optimum parameter values, the total CPU time would be 100 minutes.

Example Problem	Lower Bound	Starting Guess	Upper Bound	Number of Trials	CPU Time Required
III	XL	XS	XU		
b (pseudo)	-300	-34.3	-3	55	7min03sec
c	.001 .01	.01 .1	0.1 1.0	225 225	24min53sec 24min53sec
d	400 400 90 90 $3.4 \times 10^6$	450 450 95 95 $3.5 \times 10^6$	500 500 100 100 $3.5 \times 10^6$	2,000	68min
e	10 40 400 .3 1150	20 50 500 .5 1300	30 60 600 .55 1400	230	4hr

Table III

Table III presents a summary of the search zones and times required to obtain a solution for some of the problems considered in this thesis. The amount of CPU time required for a solution, especially for problem III-E, may seem excessive. However, there are several considerations which should be made prior to arriving at this conclusion.

- (1) The equations of the system do not have to be written, programmed nor debugged if the system's

component transfer functions are known.

(2) Time domain requirements do not have to be translated into frequency domain specifications for system simulation and design.

(3) A systematic search is carried out to obtain the optimum parameter settings. This assures that with valid bounds on the variables an acceptable solution will be obtained with the first optimization attempt.

The time required to perform the above steps in the design process by conventional means may result in many more hours of CPU time than if the program CADS were used from the beginning of the design process.

Several means of reducing the computer time required for optimization were previously outlined in section II. The most significant reduction is obtained by keeping the number of integrations required for system simulation to a minimum. Block diagram reduction of the system should be accomplished whenever possible. The example of the Ward Leonard drive system shown on page 26 can be reduced to the simple system shown in Figure 30 by block diagram reduction.

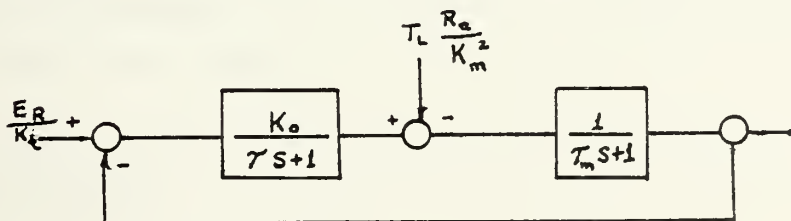


FIGURE 30 Block Reduced Ward-Leonard Drive

Section III.F. showed the effect of using different cost functions to measure the quality of the optimized response. Although the integral error squared criteria is often used to judge a system's performance, the user should carefully consider how to best define a cost function which will properly penalize deviations of the system response from the desired response. A small error ( $\text{err} < 1$ ) squared becomes even smaller. If all the errors are small, the IES is a valid cost function but if the system response involves large and small errors a weighted cost function will have to be used. One method of arriving at a properly weighted cost function is to simulate the system using first estimates of the variable parameters and recording the sum of the errors over the different portions of the response. A ratio of the errors can then be used to arrive at proper weighting factors for each time section of the response.

BOXFIX will continue the optimization process, working in the seventh significant digit until it can no longer reduce the cost function. Often an acceptable solution for the system parameters has been found long before the cost function has been reduced to its minimum. A judicious use of CADS may be made by evaluating the system response after ten to fifteen minutes of run time to see if an acceptable solution has been found.

## B. CONCLUSIONS

Time domain optimization using the CADS program is a simple, straight forward process which does not require an in-depth analysis of the system being optimized. Economic use of CPU times does dictate that intelligent starting values and bounds be placed on the variable parameters which are to be optimized.

The program is a readily usable tool for simulation without optimization. It is competitive with, if not superior to, other common simulation routines when simulating typical control systems. This feature alone is expected to bring the program into common usage.

### C. RECOMMENDATIONS FOR FUTURE WORK

(1) All integral calculations performed during this investigation were done in double precision for increased accuracy of the system response. The possibility of using single precision calculations should be investigated to decrease core requirements.

(2) The ability to begin the optimization process at some time greater than zero should be provided. This will necessitate modification of the data input cards and block equations so that initial conditions can be entered.

(3) The program presently requires that external forcing functions (LRVINS) and the variables which are to be optimized be specified by Fortran IV statements placed within the body of the program. A method of reading these specifications from data card input should be developed so that the user will not have to "shuffle" cards in the program deck.

(4) The graphical output of CADS was all that was necessary for the investigations conducted in this thesis but a provision for numerical output of selected responses should be provided for detailed analysis.

(5) The feasibility of reducing the number of significant digits ECXPLX uses should be studied as a means of reducing optimization time. Also some criteria might be developed to reject a system's response before TF is reached if it is determined to be unacceptable.

(6) A method of automatically relaxing the boundaries on the variables being optimized when they go to their limits should be developed.

(7) The standard cost function provided and all user developed cost functions should be normalized. This would permit a more direct and easier comparison of a system's "goodness" when several different integration step sizes or run times have been used in the optimization process.

## APPENDIX A

### Block Data Card Format

11            111            120            140            160

ELKCCD=EEVV            G            P            Z

CC = POSITION NUMBER OF THE BLOCK  
 C = TYPE OF BLOCK (NUMBER)  
 EE = INPUT NODE NUMBER  
 VV = OUTPUT NODE NUMBER  
 G = VALUE OF GAIN  
 P = VALUE OF THE POLE\*  
 Z = VALUE OF THE ZERO\*

\* For block type 4,  $\delta$  is read into the P location and  $\omega_n$  is read into the Z position.

\* For block type 5,  $\theta_u$  is read into the P position and  $\theta_l$  is read into the Z position.

\* For block type 6,  $\theta_c$  is read into the P position and  $\theta_g$  is read into the Z position.

#### EXAMPLES

	G	
ELK11=0102	10.	
	G      P	
BLK12=0304	1.    5.	
	G      P      Z	
BLK33=0405	1.    10.    5.	

	G	$\delta$	$\omega_N$
BLK 104=1006	200.	.2	14.14
	G	$\theta_u$	$-\theta_L$
BLK 115=1207	10.	20.	-5.
	G	$\theta_c$	$\theta_B$
BLK 126=0708	1.	3.	10.

\*See Table I.



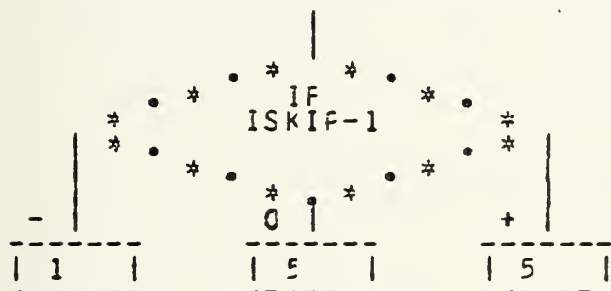
## Plant Flow Chart

```

FUNCTION FLANT (C)
  DIMENSION G(25), P(25), Z(25), FLAG(25,25), CM
  G(25), THACCT(25), CMGDOT(25), DRVIN(25),
  NF(25), IR(25), IV(25), X2(25), X2DOT(25),
  CRIVE(25), THA(25), IC(25), ID(25), IE(25),
  THACUT(3001), XCATA(3001), C(25)

  REAL *8THACUT
  REAL *8XCATA
  REAL *8THA,THACOT,T,DT,CRIVE,CMG,CMGDOT,DRVIN,TF
  REAL *8F1,F2
  REAL *8X2,X2DOT
  COMMON T,DT,TF,THACUT,XDATA,M3,ICCNT,NEG,ISKIP,ITF
  FOR OPT RUNS, INHIBIT READ STATEMENTS AFTER READING

```



1 ISKIP=2

```
***READ (5,24) N, ISET
INITIALIZE COUNTERS
```

ICUT = 0  
IVOLT = 0  
F1 = 0  
F2 = 0.500 \* F1  
A11 = 0  
A55 = 0  
A66 = 0  
ICK = 0.4

FEAC INFLT DATA

+ 22

$$I = 1, N$$

```
***READ (5,25) IC(I),ID(I),IE(I),IV(I),G(I),P(I),Z(I)
```

```
SET TRACUT = CUTPLT CF LAST BLOCK
```

F

\* (IV(I)-IV(CT)).LE.O \*

T 1 2

F

$$\begin{aligned} \text{IVCLT} &= \text{IV}(\text{I}) \\ \text{ICLT} &= \text{IC}(\text{I}) \end{aligned}$$

F

IC (I)

T | N11=N11+1

三

IC (I)

T | N55=N55+1

三

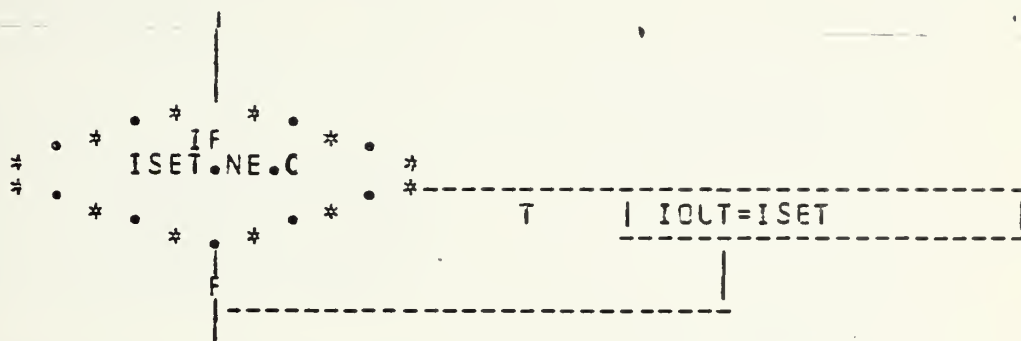
IC (I) I

$$T \quad | \quad N \in \mathcal{C} = N \in \mathcal{C} + 1$$

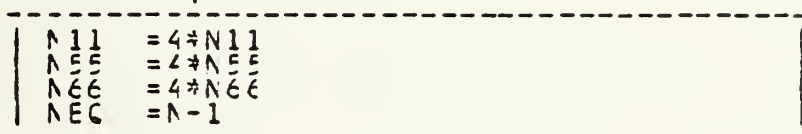
14

```
3      +++++*WRITE (6,26) IC(I),IC(I),IE(I),IV(I),G(I),P(I),Z(I)
```

SET THACLT = SPECIFIED THETA, IF ANY

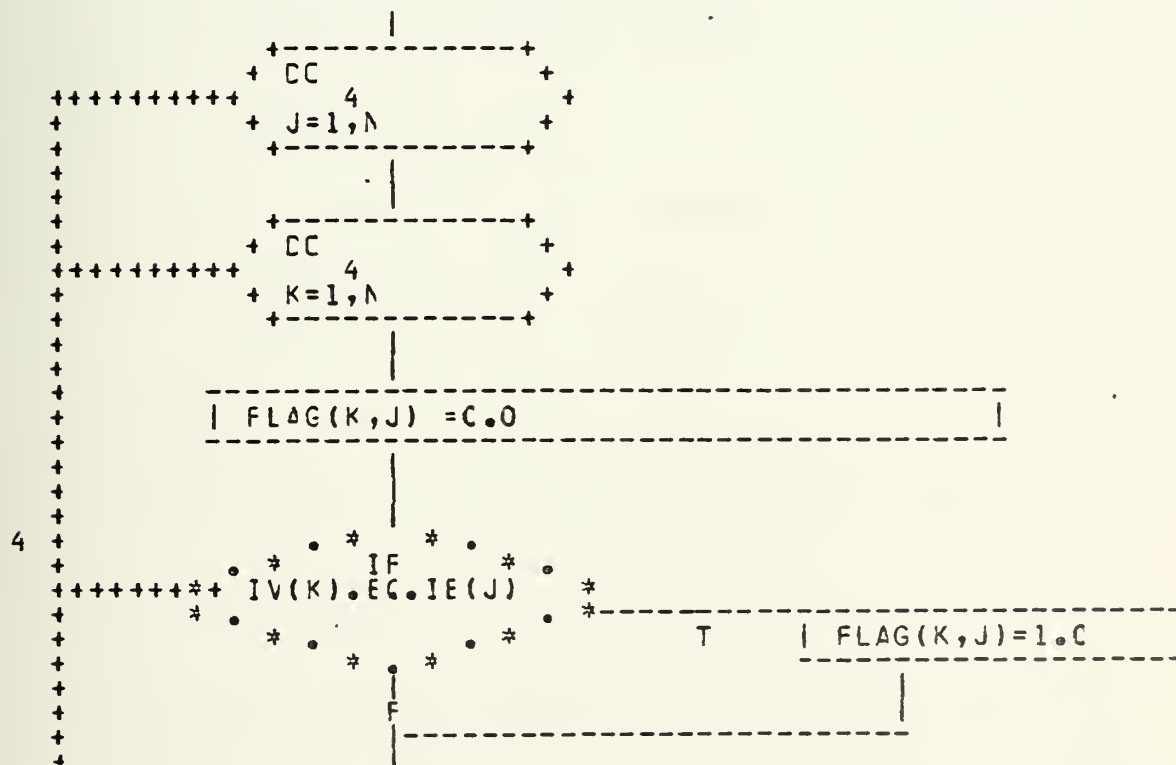


\*\*\*WRITE (6,27) IOUT



SCAN FOR INPLTS

CONNECT SYSTEM BY SETTING FLAG=1. FOR CONNECTED BLKS



TAKE BLK TYPE AND SOLVE EGNS ONE BY ONE

# CLEARING CLT REGISTERS AND INITIALIZING COUNTERS

```

5      +-----+
      + DO
      + ICLR=1,N
      +-----+
      |
      | THA(ICLR) =0.00
      | THACOT(ICLR) =0.00
      | CMG(ICLR) =0.00
      | CMGDOT(ICLR) =0.00
      | CFVIN(ICLR) =0.00
      | X2(ICLR) =0.00
      |-----|
6      +-----+
      | X2DOT(ICLR) =0.00
      | 1 =0.000
      |-----|

```

NR'S CONTROL ENTRY PCINT IN INTEGRATION SUBROUTINES

```

      |-----|
      | NR2 =1
      | NR3 =1
      | NR4 =1
      |-----|

```

M2 CONTROLS WHICH BLOCK EQUATION IS BEING SOLVED

```

      |-----|
      | M2 =0
      |-----|

```

ICCNT IS USED TO CONTROL PROGRAM FLOW

```

      |-----|
      | ICCNT=0
      |-----|

```

IWAIT IS USED TO CONTROL TIME. TIME IS STEPPED EVERY  
FIRST AND THIRD PASS THRU INTEGRATION ROUTINES

```

      |-----|
      | IWAIT=0
      | IT =0
      |-----|

```

ILAST'S CONTROL PROGRAM DATA AND PROGRAM EXIT

```

      |-----|
      | ILAST=0
      | IELAST =0
      | IELAST =0
      |-----|

```

SET DRIVES FOR INFLTS

```

7      +-----+
      + CC          +
      ++++++++      +
      + MDRV=1,N    +
      +-----+
      |
      +-----+
      | CRVIN(1) = 1.
      | CRIVE(MDRV) = 0.00
      +-----+
      |
      +-----+
      + CC          +
      ++++++++      +
      + M=1,N       +
      +-----+
      |
      +-----+
8  ++++++++ | CRIVE(MDRV) = CRIVE(MDRV) + TFA(M)
      +-----+
      |
      +-----+
9  ++++++++ | CRIVE(MDRV) = CRVIN(MDRV) + CRIVE(MDRV)
      +-----+
      |
10  +-----+
      | M2 = M2+1

```

FICK TYPE EGN TC SOLVE

[illegible]



SCLVES THACT = C\*THAIN

```

TFA(M3) = C(M3)*CFIVE(M3)
IWAIT=IWAIT+1
ILAST=ILAST+1

```

```
*      *      *      *      *
*      *      IF      *      *
*(ILAST.EC.N11).AND.(ICGNT.EC.NEQ)
*      *      *      *      *
*      *      T      | 21
*      *      *      *      *
*      *      F
*      *      |
*      *      | 18 |
```

SOLVES  $T_{FACLT}/T_{FAIN} = G/(S + P)$

```

      TFADOT(M3) = -P(M3)*TFA(M3)+G(M3)
      *CRIVE(M3)
      S      =FKLCE2(TFA,TFADOT,NR2)
      IWAIT=IWAIT+1

```

IF  
S-1.0  
C

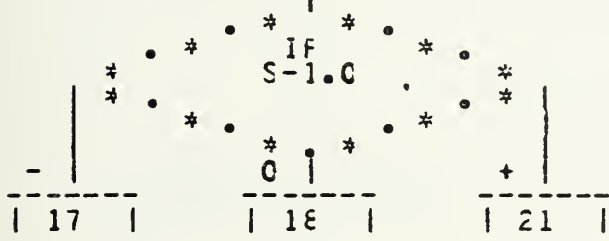
SOLVES THAOLY/THAIN = G\*(S + Z)/(S + P)

```
CMGDOT(M3) = -P(M3)*CMG(M3)+G(M3)
             *FIVE(M3)
```



S=RKLDE3(CMG,CMGDCT,NR3)

THA(M3) = (Z(M3)-F(M3))\*OMG(M3)  
+G(M3)\*DRIVE(M3)  
IWAIT=IWAIT+1

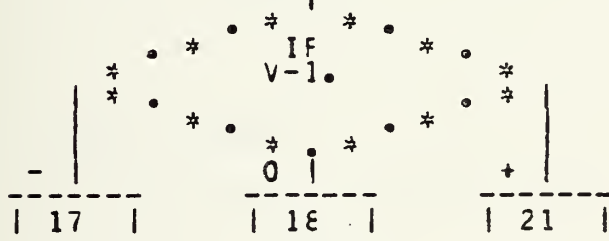


TYPE FOUR EGNS.

SOLVES THACLT/THAIN = G/(S\*\*2 + 2\*DELTA\*WN\*S + WN\*\*2)

14

V = CCFLX(F,Z,G,DRIVE,X2,CMG,NR4)  
THA(M3) = CMG(M3)  
IWAIT=IWAIT+1

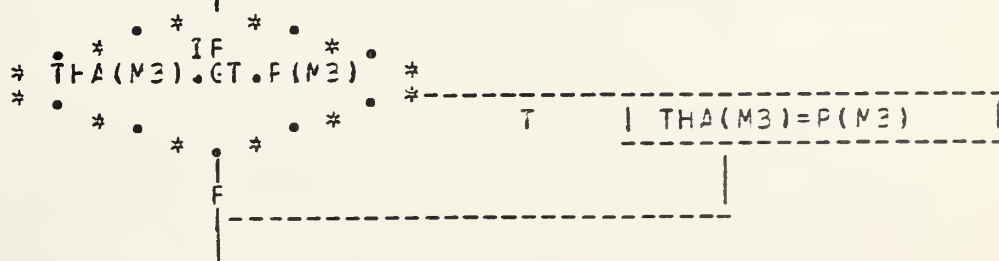


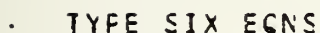
TYPE FIVE EGNS

SOLVES THACLT = G\*THAIN FOR /G\*THAIN/ < SAT LIMITS

15

THA(M3) = G(M3)\*DRIVE(M3)





14



```
17      ***WRITE (6,29)
          STOP
```

IF  
ICCN-T-M

0

10 15 20

```

19      | NR2 = NR2 + 1
      | NR3 = NR3 + 1
      | NR4 = NR4 + 1
      | NR5 = C
      | ICNT = 0

```

```
20      ***WRITE (6,30)
          STEP
```

```

      IT=IT+1
      THACUT(IT)=THA(IOUT)

```

```

22      NR2      = 1
        NR3      = 1
        NR4      = 1
        ME        = C
        ICCNT     = C
        IWAIT     = C
        ILAST     = C
        ISLAST    = 0
        IELAST    = 0

```

1 7 1

23 | FLANT=1. |

```

24      FORMAT (I2,2X,I2)
25      FORMAT (3X,I2,I1,1X,2I2,8X,3E20.7)
26      FORMAT (/ ,5F BLK ,I2,I1,2H =,2I2,6X,3E20.7)
27      FORMAT (//,2X,'THETA CUT IS THA(',I2,')')
28      FORMAT (4CH *** EQN SWITCH CONTROL DID NOT WORK)
29      FORMAT (2CH INTEGRATION TROUBLE)
30      FORMAT (58F ERROR IN INTERGATION. ATTEMPTED TO
      INTEG. MORE THAN N-EQN)

```

79

# APPENDIX C

```

C      DECK MODIFIED FOR PROBLEM III-E.
C      MODIFICATIONS TO MAIN
C      CALCULATE STANDARD SECCNC ORDER SYSTEM RESPONSE FOR BOXPLS DATA
C      XCC = -2*E*WN*XD - WN**2*X + DRV
C      ICATA = 0
C      X(1) = 0.00
C      DO NOT COMPUTE DATA CURVE IF LEAP = 1
C      IF (LEAP.EC.1) GO TO 5
C      X(2) = 0.00
C      NT = 0
C      T = T+DT
C      IF (T.GE.0.13) GO TO 1813
C      IF (T.GE.0.1) GO TO 1812
C      IF (T.GE.0.0236) GO TO 1811
C      X(1) = 1247.46*T
C      GO TO 1814
C      X(1) = 31.8
C      GO TO 1814
C      X(1) = 31.8-1060.*(T-0.1)
C      GO TO 1814
C      X(1) = 0.
C      ICATA = ICATA+1
C      XDATA(ICATA) = X(1)
C      IF (T-TF) 181, 183, 183
C      NOW HAVE STANDARD VALUES
C      CONTINUE
C      CONTINUE WITH PROB
C      MODIFICATIONS TO PLANT
C      7 CC 5 MCRV=1,N
C      CRV IN(I)'S GO HERE IF FUNCTIONS OF TIME
C      8888
C      THA12 = T+A(12)
C      INCRV = INT(THA12)
C      CRV IN(2) = FLOAT(INCRV)
C      IF (IWAIT.EC.0) T = T+H2
C      IF (T.GE.0.13) GO TO 1122
C      IF (T.GE.0.1) GO TO 1123
C      IF (T.GE.0.0236) GO TO 1124
C      CRV IN(1) = 1247.46*T

```

1900  
1910  
1920  
1930  
1940  
1950  
1960  
1970  
1980  
1990  
2000  
2010

1290  
1300  
1310  
1320

```

1124 GC TO 1125
      CRVIN(1)=31.8
1125 GC TO 1125
1126 CRVIN(1)=31.8-1060.*(7-0.1)
1127 GC TO 1125
1128 CRVIN(1)=0.0
      CCNTINUE
      IF(T.LT.0.0236) GC TO 1126
      IF(T.GT.0.1) GC TO 1127
1129 GC TO 1128
      CRVIN(5)=2.809
1130 GC TO 1129
      IF(T.GT.0.13) GC TO 1128
1131 CRVIN(5)=-2.809
      GC TO 1129
      CRVIN(5)=0.
      CCNTINUE
      IF(T.LT.0.0236) GC TO 1130
      IF(T.GT.0.1) GC TO 1131
1132 CRVIN(4)=0.9839
      GC TO 1132
      CRVIN(4)=41.6522*T
1133 GC TO 1132
      IF(T.GT.0.13) GC TO 1133
1134 CRVIN(4)=0.9839+32.7578*(0.1-T)
      GC TO 1132
      CRVIN(4)=0.
      CCNTINUE
      CRIVE(MCRV) = 0.00
      CC 8 M=1,N
      CRIVE(MCRV) = DRIVE(MDRV)+THA(M)*FLAG(M,MDRV)
      CRIVE(MCRV) = DRVIN(MDRV)+DRIVE(MCRV)

```

```

1330
1340
1350
1360
1370
1380
1390
1400

```

// EXEC FCRTCLG,REGION.GO=200K

//FCRTSYSIN DD \*

COMPUTER AUTOMATED DESIGN OF SYSTEMS  
(CACCS)

BY  
LARRY PAUL VINES  
LIEUTENANT USN

1 APRIL 76

THIS PROGRAM WILL SIMULATE/OPTIMIZE CONTROL SYSTEMS AND CIRCUITS.  
THE INPUT DATA IS IN TRANSFER FUNCTION BLOCKS. FORMATION TO SIMULATE  
THE SYSTEM WHICH IS TO BE OPTIMIZED. TRANSFER FUNCTIONS WHICH  
ARE COMMONLY ENTERED WERE THEN PROGRAMMED IN AN ARBITRARY  
FACILITATION FROM THE DATA CARD INPUT. SEVERAL BLOCKS PREVIOUSLY  
TRANSFERRED TO SIMULATE MOST CONTROL SYSTEMS. TO BE EASILY  
ADAPTED FOR A WITH THE KNOWN SYSTEM PARAMETERS AND BY THE RESPONSE.  
ALL UNKNOWN OR ADJUSTABLE PARAMETERS TO BE DESIRED SYSTEM  
MINIMIZATION OUTPUT OF THE DESIRED RESPONSE AND ACTUAL SYSTEM  
RESPONSE IS THEN PROVIDED.

DESCRIPTION OF PARAMETERS

NRUNS = NUMBER OF RUNS TO BE MADE. NRUNS = 1 WHEN OPTIMIZING.

NV = NUMBER OF VARIABLES BOXPLX WILL SET.

NAV = NUMBER OF AUX VARIABLES DEFINED.

LEAF = 0 COMPUTES STANDARD SECOND ORDER STEP RESPONSE FOR  
DATA CURVE.

= 1 SKIPS SECOND ORDER DATA EQUATION

NFR = FREQUENCY OF OUTPUT FROM BOXPLX FOR DIAGNOSTIC PURPOSES.  
(NPR = 25, 50, 100 IS RECOMMENDED)



```

NTA = NUMBER OF TRAILS ALLOWED BY BOXPLX FOR A SOLUTION.
IFLCT = OPTIONAL PRINTER PLOT OF SOLUTION.
        = 1 PRODUCES PLOT. = 0 NO PLOT.
ICRAW = OPTIONAL CALCOMP GRAPH OF SOLUTION.
        = 1 PRODUCES PLOT. = 0 NO PLOT.
** ONLY ONE PLOT OPTION MAY BE USED AT A TIME. ICFW REQUIRES
   A //EXEC CLGP CONTROL CARD AND 230K REGION.
T = TIME INITIAL CONDITION. MUST BE ZERO.
CT = STEP SIZE FOR INTEGRATION. TF/1000. IS RECOMMENDED.
TF = FINAL PROBLEM TIME.
DELTA = CAMPING FACTOR
WN = NATURAL FREQUENCY
BETA = GAIN FACTOR
XS(I) = STARTING GUESS
XL(I) = UPPER BOUND
XL(I) = LOWER BOUND
N = NUMBER OF TRANSFER FUNCTION BLOCKS CONNECTED.
ISET = OUTPUT VARIABLE TO BE OPTIMIZED/PLOTTED.
      DEFAULT VARIABLE PLOTTED IS HIGHEST NUMBERED NODE VAR.

DESCRIPTION OF BLOCK TRANSFER FUNCTIONS
BLKCCD=EEVV      G      P/DELTA/UL/REF      Z/WN/LL/BOUND
CC = NUMBER OF BLOCK IN SYSTEM CONFIGURATION (IE. BLK NUMBER 1)
C = TYPE OF TRANSFER FUNCTION BLOCK.
EE = INPUT NODE NUMBER
VV = OUTPUT NODE NUMBER
G = GAIN OF BLOCK
P = PCLE OF BLOCK TRANSFER FUNCTION
DELTA = CAMPING FACTOR FOR COMPLEX TRANSFER BLOCK (TYPE 4)

```



```

DIMENSION THAOUT(3001), XDATA(2001)
REAL *8XDATA
REAL *8THAOUT
REAL *8X,XDOT,T,TF,CT
REAL *8TF
COMMON T,DT,TF,THAOUT,XDATA,M3,ICCNT,NEQ,ISKIP,ITF
THE MULTIPLE RUN OPTION SHOULD NOT BE USED WHEN EMPLCYING
BCXPLX. TIME BECOMES EXCESSIVE. USE ONLY FOR PLANT - DATA RUNS

READ (5,12) NRUNS
READ/WRITE CONTROL DATA

CC 11 IRUN=1,NRUNS
READ (5,13) NV,NAV,LEAP,NPR,NTA,IPLOT,IDRAW
WRITE (6,14) NV,NAV,LEAP,NPR,NTA
READ (5,15) T,DT,TF
WRITE (6,16) T,DT,TF
READ (5,15) DELTA,WN,BETA
WRITE (6,17) DELTA,WN,BETA

READ/WRITE SEARCH BOUNDS IF OPTIMIZING
IF (NV.EC.O) GO TO 1
SET LIMITS
STARTING GUESS
READ (5,18) (XS(I),I=1,NV)
LPPER BCUNC
READ (5,18) (XU(I),I=1,NV)
LCWER BCUNC
READ (5,18) (XL(I),I=1,NV)
WRITE (6,15)
WRITE (6,20) (XS(I),I=1,NV)
WRITE (6,21)
WRITE (6,20) (XU(I),I=1,NV)
WRITE (6,22)
WRITE (6,20) (XL(I),I=1,NV)
CCCN INUE
1 ICLP = TF/DT
ITF = ICF
IF (ICLP.GT.4500) IDP=4500

```

CCCC

CCCC

CCC

CCCC

CC

CC

C

```

C      PLCT EVERY FIFTH DATA PCINT
C
C      NFFLT = 0.2*IDP
C      R = 1./2.
C      IF = 0
C      ISKIP = 0
C
C      CALCULATE STANDARD SECONC ORCER SYSTEM RESPNCSE FCR BOXFLS DATA
C      XCC = -2*E*WN*XD - WN**2*X + DRV
C
C      ICATA = 0
C      X(1) = 0.00
C
C      CC NCT COMPUTE DATA CURVE IF LEAF = 1
C
C      IF (LEAF.EQ.1) GO TO 5
C      X(2) = 0.00
C      NT = 0
C      2 XCCCT(1) = X(2)
C      XCCCT(2) = -2.*DELTA*WN*X(2)-WN**2*X(1)+BETA
C      S = RKLCEQ(2,X,XDOT,T,CT,NT)
C      IF (S-1.) > 2,4
C      3 WRITE (6,23)
C      STCP
C
C      4 ICATA = IDATA+1
C      XCATA(ICATA) = X(1)
C
C      TEST FOR END OF CCMPUTATION
C
C      IF (T-TF) 2,5,5
C      NOW HAVE STANDARD VALUES      CONTINUE WITH PROE
C      CCNTINUE
C
C      SET DATA CURVE = 0. IF NOT FLOTTING
C
C      IF (LEAF.EQ.0) GO TO 7
C
C      CC 6 I=1,4500
C      ICATA = IDATA+1
C      T = T+DT
C      XCATA(ICATA) = X(1)
C      IF (T-TF) 6,7,7
C      CCNTINUE
C
C      CALL PLANT TO SIMULATE THE SYSTEM
C
C

```

```

C      7 IF (NV.EC.0) PL = PLANT(1.)
C      IF (NV.EC.0) GO TO 8
C
C      IF OPTIMIZING, CALL BCXPLX AND WRITE OPTIMIZED VALUES
C
C      CALL BOXPLX (NV,NAV,NPR,NTA,R,XS,IP,XU,XL,YMN,IER)
C      WRITE (6,24) (XS(I),I=1,NV)
C      WRITE (6,25) YMN,IER
C
C      PLCT SYSTEM RESPONSE
C
C      8 IF (IFLCT.EC.0) GO TO 9
C      WRITE (6,26)
C      CALL FPLT (XDATA,THAOUT,DT,NPPLT,IDP)
C      GO TO 11
C
C      9 IF (ICRAW.EC.0) GO TO 10
C      CALL PIC (XDATA,THAOUT,DT,NPPLT,ICP)
C      GO TO 11
C
C      10 WRITE (6,27)
C      11 WRITE (6,28) IRUN
C
C      STCP
C
C      12 FCRMAT (I1)
C      13 FCRMAT (I1)
C      14 1, I5, 2X, 'NV = ', I5, 2X, 'NAV = ', I5, 2X, 'LEAP = ', I1, 2X, 'NFR = '
C      15 1, I5, 2X, 'NTA = ', I5)
C      16 FCRMAT (I1)
C      17 FCRMAT (I1)
C      18 FCRMAT (I1)
C      19 FCRMAT (I1)
C      20 FCRMAT (I1)
C      21 FCRMAT (I1)
C      22 FCRMAT (I1)
C      23 FCRMAT (I1)
C      24 FCRMAT (I1)
C      25 FCRMAT (I1)
C      26 FCRMAT (I1)
C      27 FCRMAT (I1)
C      28 FCRMAT (I1)
C      29 FCRMAT (I1)
C      30 FCRMAT (I1)
C      31 FCRMAT (I1)
C      32 FCRMAT (I1)
C      33 FCRMAT (I1)
C      34 FCRMAT (I1)
C      35 FCRMAT (I1)
C      36 FCRMAT (I1)
C      37 FCRMAT (I1)
C      38 FCRMAT (I1)
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C      40 FCRMAT (I1)
C      41 FCRMAT (I1)
C      42 FCRMAT (I1)
C      43 FCRMAT (I1)
C      44 FCRMAT (I1)
C      45 FCRMAT (I1)
C      46 FCRMAT (I1)
C      47 FCRMAT (I1)
C      48 FCRMAT (I1)
C      49 FCRMAT (I1)
C      50 FCRMAT (I1)
C      51 FCRMAT (I1)
C      52 FCRMAT (I1)
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C      62 FCRMAT (I1)
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C      65 FCRMAT (I1)
C      66 FCRMAT (I1)
C      67 FCRMAT (I1)
C      68 FCRMAT (I1)
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C      78 FCRMAT (I1)
C      79 FCRMAT (I1)
C      80 FCRMAT (I1)
C      81 FCRMAT (I1)
C      82 FCRMAT (I1)
C      83 FCRMAT (I1)
C      84 FCRMAT (I1)
C      85 FCRMAT (I1)
C      86 FCRMAT (I1)
C      87 FCRMAT (I1)
C      88 FCRMAT (I1)
C      89 FCRMAT (I1)
C      90 FCRMAT (I1)
C      91 FCRMAT (I1)
C      92 FCRMAT (I1)
C      93 FCRMAT (I1)
C      94 FCRMAT (I1)
C      95 FCRMAT (I1)
C      96 FCRMAT (I1)
C      97 FCRMAT (I1)
C      98 FCRMAT (I1)
C      99 FCRMAT (I1)
C      100 FCRMAT (I1)
C
C      KE EVALUATES IMPLICIT CONSTRAINTS ON BOXPLX VARIABLES
C      FUNCTION KE (C)
C      DIMENSION C(25)

```



```

C      NC IMPLICIT CONSTRAINTS
C      KE = 0
C      RETURN
C      ENC
C
C      FE COMPUTES THE ERROR FUNCTION(PERFORMANCE INDEX) FOR BOXPLX
C      FUNCTION FE (C)
C      DIMENSION THAOUT(3001), XDATA(3001), C(25)
C      REAL *8XDATA,THAOUT,CT,T,DIFF,PI
C      REAL *8TF
C      COMMON T,DT,TF,THAOUT,XDATA,M3,ICCNT,NEQ,ISKIP,ITF
C      THAOUT(1) = 0.00
C      DIFF = 0.00
C      PI = 0.00
C      PL = PLANT(C)
C
C      CC 1 I=1,ITF
C      DIFF = XDATA(I)-THAOUT(I)
C      1 PI = PI+DIFF**2
C
C      VALUE OF P I
C      FE = PI
C      RETURN
C      ENC
C
C      FUNCTION PLANT SIMULATES THE SYSTEM
C
C      FUNCTION PLANT (C)
C      DIMENSION G(25), P(25), Z(25), FLAG(25,25), CRIVE(25), THA(25), OM
C      IC(25), THADOT(25), CMGDOT(25), CRVIN(25), IC(25), IE(25),
C      2NF(25), IR(25), IV(25), X2(25), X2DOT(25), THAOUT(3001), XDATA(300
C      =1), C(25)
C      REAL *8THAOUT
C      REAL *8XDATA
C      REAL *8THA,THADOT,T,DT,DRIVE,OMG,CMGDOT,CRVIN,TF
C      REAL *8F1,F2
C      REAL *8X2,X2DOT
C      COMMON T,DT,TF,THAOUT,XDATA,M3,ICCNT,NEQ,ISKIP,ITF
C      FOR OPTIMIZATION RUNS INHIBIT READ STATEMENTS AFTER READING
C
C      IF (ISKIP-1) 1,5,5
C      1 ISKIP = 2
C      READ (5,24) N,ISET
C
C      INITIALIZE COUNTERS

```

```

ICUT = 0
IVCUT = 0
PI = DT
PI = 0.500*H1
N11 = 0
N15 = 0
N66 = 0
ICK = 2*N

**READ INPUT DATA**
COMPLEX BLOCK IN Z FIELD 44 READS DELTA IN FROM P FIELD AND
SATURATION BLOCK TYPE 55 READS PLUS SAT LEVEL IN FROM P FIELD AND
NEG SAT LEVEL FROM Z FIELD
DEAD ZONE BLOCK TYPE 6 READS CONTROL REF FROM P FIELD AND
DEAD ZONE BOUND FROM Z FIELD

CC 3 I=1,N
READ (5,25) IC(I),ID(I),IE(I),IV(I),G(I),P(I),Z(I)
SET THACUT = OUTPUT OF LAST BLOCK
IF ((IV(I)-IVOUT).LE.0) GO TO 2
ICUT = IV(I)
ICUT = IC(I)
IF (IC(I).EQ.1) N11=N11+1
IF (IC(I).EQ.5) N15=N15+1
IF (IC(I).EQ.6) N66=N66+1
2

3 WRITE (6,26) IC(I),ID(I),IE(I),IV(I),G(I),P(I),Z(I)

SET THACUT = SPECIFIED THETA, IF ANY
IF (ISET.NE.0) IOUT=ISET
WRITE (6,27) IOUT
N11 = 4*N11
N15 = 4*N15
N66 = 4*N66

** SHOULD NOW HAVE INPUT DATA AVAILABLE IN C,D,E,V ***
NEC = N-1
*** SCAN FOR INPUTS ***

```

CCCCCCCCCCCC CCCC CCCCCC CCCC CCCC



```

CC CONNECT UP SYSTEM BY SETTING FLAG=1. IF BLOCKS ARE CONNECTED
CC
CC 4 J=1,N
CC 4 K=1,N
CC FLAG(K,J) = 0.0
4 IF (IV(K).EQ.IE(J)) FLAG(K,J)=1.0
CC
CC **NOW MUST TAKE TYPE OF BLK AND GC TO ECNS FOR SOLUTION**
CC BY SOLVING BLCK BY BLOCK
CC
CC CLEARING OUT REGISTERS AND INITIALIZING COUNTERS
CC
5 CC 6 ICLR=1,N
CC TFA(ICLR) = 0.00
CC TFCOT(ICLR) = 0.00
CC CMG(ICLR) = 0.00
CC CMGOT(ICLR) = 0.00
CC CFVIN(ICLR) = 0.00
CC X2(ICLR) = 0.00
CC X2COT(ICLR) = 0.00
CC
CC T = C.000
CC
CC NF'S CONTROL ENTRY PCINT IN INTEGRATION SUBROUTINES(RKLCDE'S)
CC
CC NF2 = 1
CC NF3 = 1
CC NF4 = 1
CC
CC M3 CONTROLS WHICH BLOCK EQUATION IS BEING SOLVED
CC
CC M3 = 0
CC
CC ICCNT IS USED TO CONTROL PROGRAM FLOW
CC
CC ICCNT = 0
CC
CC IWAIT IS USED TO CONTROL TIME. TIME IS STEPPED EVERY FIRST AND
CC THIRD PASS THRU INTEGRATION ROUTINES
CC
CC IWAIT = 0
CC IT = 0
CC
CC ILAST'S CONTROL PROGRAM DATA AND PROGRAM EXIT

```

```

C      ILAST = 0
C      IELAST = 0
C      IELAST = 0
C      SPECIFY ANY PARAMETERS TO BE OPTIMIZED
C      EC. P(1)=C(2), Z(1)=C(1),
C      ** INSERT NV VARIABLE SPECIFICATIONS HERE **
C      G(1)=C(1)
C      **SET DRIVES FOR INPUTS**
C      CFVIN(1)=1.
C
C      7 CC 9 MCRV=1,N
C      CFVIN(I)'S GO HERE IF FUNCTIONCS CF TIME
C      DRIVE(MCRV) = 0.00
C
C      8 CC 8 N=1,N
C      DRIVE(MCRV) = DRIVE(MDRV)+T+A(M)*FLAG(M,MCRV)
C
C      9 CFIVE(MCRV) = DRVIN(MCRV)+DRIVE(MCRV)
C
C      10 N3 = M3+1
C
C      PICK TYPE EQN TO SOLVE
C      IF (IWAIT.EQ.0) T = T+H2
C      IF (IC(M3).EQ.1) GC TO 11
C      IF (IC(M3).EQ.2) GC TO 12
C      IF (IC(M3).EQ.3) GC TO 13
C      IF (IC(M3).EQ.4) GC TO 14
C      IF (IC(M3).EQ.5) GC TO 15
C      IF (IC(M3).EQ.6) GC TO 16
C      WRITE (6,28)
C      STCP
C
C      **START SOLUTION**
C      TYPE CNE EQUATIONS
C      SCLVES THACUT = G*THAIN
C
C      11 T+A(M3) = G(M3)*DRIVE(M3)
C      IWAIT = IWAIT+1

```

```

1630 ILAST = ILAST+1
1640 IF ((ILAST.EQ.N11).AND.(ICONT.EC.NEQ)) GO TO 21
1650 GC TO 18
1660
1670 TYPE TWO EQNS
1680 SCLVES THAOUT/THAIN = G/(S + P)
1690
1700 12 THACOT(M3) = -P(M3)*TFA(M3)+G(M3)*DRIVE(M3)
1710
1720 S = RKLCE2(TFA,THACOT,NR2)
1730 IWAIT = IWAIT+1
1740 IF (S-1.0) 17,18,21
1750
1760 TYPE THREE EQNS
1770 SCLVES THAOUT/THAIN = G*(S + Z)/(S + P)
1780
1790 13 CMGDOT(M3) = -P(M3)*OMG(M3)+G(M3)*DRIVE(M3)
1800 S = RKLCE3(OMG,OMGDOT,NR3)
1810 TFA(M3) = (Z(M3)-P(M3))*CMG(M3)+G(M3)*DRIVE(M3)
1820 IWAIT = IWAIT+1
1830 IF (S-1.0) 17,18,21
1840
1850 TYPE FOUR EQNS
1860 SCLVES THAOUT/THAIN = G/(S**2 + 2*DELTA*WN*S + WN**2)
1870
1880 14 V = CCPLX(P,Z,G,DRIVE,X2,OMG,NR4)
1890 TFA(M3) = CMG(M3)
1900 IWAIT = IWAIT+1
1910 IF (V-1.) 17,18,21
1920
1930 TYPE FIVE EQNS
1940 SCLVES THAOUT = G*THAIN FOR /G*THAIN/ < SATURATION LIMITS
1950
1960 15 TFA(M3) = G(M3)*DRIVE(M3)
1970 IF (TFA(M3).GT.P(M3)) TFA(M3)=P(M3)
1980 IF (TFA(M3).LT.Z(M3)) TFA(M3)=Z(M3)
1990 IWAIT = IWAIT+1
2000 IELAST = IELAST+1
2010 IF ((IELAST.EQ.N55).AND.(ICONT.EC.NEQ)) GC TO 21
2020 GC TO 18
2030
2040 TYPE SIX EQNS
2050 SCLVES THAOUT = G*THAIN FOR CCNTROL REF > BOUND DEAD SPACE
2060
2070 16 TFA(M3) = G(M3)*DRIVE(M3)
2080 IF = P(M3)
2090 IF ((CABS(TFA(IP)))*LT.Z(M3)) TFA(M3)=0.
2100 IWAIT = IWAIT+1

```

```

16LAST = I6LAST+1
IF ((I6LAST.EQ.N66).AND.(ICCNT.EC.NEQ)) GO TO 21
C
17 WRITE (6,25)
STOP
18 ICCNT = ICCNT+1
IF (ICONT-N) 10,19,20
C
CNE PASS HAS BEEN MADE FOR EACH ECN. GO TO NEXT STEP INCREMENT
C
19 NF2 = NF2+1
NF3 = NF3+1
NF4 = NF4+1
N3 = 0
ICCNT = 0
IF (IWAIT.EQ.ICK) IWAIT=0
GO TO 7
C
20 WRITE (6,30)
STOP
C
CATA COLLECTION PCINT. DATA IS RECORDED AT END CF COMPLETE
TIME STEP(CT)
C
21 IT = IT+1
THACUT(IT) = THA(IOUT)
TEST FOR END OF RUN
C
IF (T-TF) 22,22,23
RESET CCOUNTERS FOR NEXT PASS THRU EQUATIONS
22 NF2 = 1
NF3 = 1
NF4 = 1
N3 = 0
ICCNT = 0
IWAIT = 0
I6LAST = 0
I6LAST = 0
GO TO 7
23 RETURN
C
24 FORMAT (12,2X,12)
25 FORMAT (3X,12,11,1X,212,8X,3E20,7)
26 FORMAT (/ ,5H BLK ,12,11,2H =,212,6X,3E20,7)
27 FORMAT (//,2X,1THETA CUT IS THA( ,12, ,))

```

2550  
2600  
2610  
2620  
2630

```

26 FCFMAT (40F *** EGN SWITCH CONTRCL DID NOT WORK ***)
25 FCFMAT (20F INTEGRATION TROUBLE)
30 FCFMAT (58H ERROR IN INTERGATION. ATTEMPTED TO INTEG. MORE THAN N-
1 EGN)
ENC

```

C  
C  
C  
C  
C

```

      FORTRAN 4 VERSION OF RUNGE-KUTTA-GILL ROUTINE
      X,XDOT,T,DT, ARE IN DOUBLE PRECISION
      MAX N=25

```

```

      FUNCTION RKLDEQ(N,X,XDOT,T,DT,NT)
      REAL*8 X,XDOT,T,DT,C,H1,H2,H3,H4
      DIMENSION X(1),XDOT(1),C(25)

```

C

```

      NT = NT + 1
      GO TO (1,2,3,4),NT
1 F1 = DT
  F2 = F1*0.500
  F3 = F1*2.000
  F4 = F1/6.000
  CC 11 J = 1,N
11 C(J) = 0.00
  A = 0.500
  T = T + H2
  GO TO 5

```

C

```

2 A = 0.2528932188134525
  GO TO 5

```

C

```

3 A = 1.7071067811865475
  T = T + H2
  GO TO 5

```

C

```

4 CC 41 I = 1,N
41 X(I) = X(I) + H6*XDOT(I) - Q(I)/3.00
  AT = 0
  RKLCEG = 2.
  GO TO 6

```

C

```

5 CC 51 L = 1,N
51 X(L) = X(L) + A*(CT*XDOT(L)-Q(L))
  C(L) = F3*A*XDOT(L) + (1.00 - 3.00*A)*Q(L)
  RKLCEG = 1.

```

C

```

6 RETURN
  ENC

```

C  
C

```

      FORTRAN 4 VERSION OF RUNGE-KUTTA-GILL ROUTINE

```

2640  
10

C  
C  
C

X,XDOT,T,DT, ARE IN DOUBLE PRECISION  
MAX N=25

```

FUNCTION RKLDE2 (X,XDOT,NR2)
DIMENSION X(4), XDOT(4), Q(25)
DIMENSION THAOUT(3001), XDATA(3001)
REAL *8THAOUT,XDATA
REAL *8X,XDOT,T,DT,C,H1,H2,H3,H6
REAL *8ITF
COMMON T,DT,TF,THAOUT,XDATA,M3,ICCNT,NEQ,ISKIP,ITF

```

C

```

      GC TO (1,2,3,4), NR2
1  IT = DT
   IT = H1*0.5D0
   IT = H1*2.0D0
   IT = H1/6.0D0
   C(M3) = 0.0D0
   A = 0.5D0
      GC TO 5

```

C

```

2  A = 0.2528532188134525
      GC TO 5

```

C

```

3  A = 1.7071067811865475
      GC TO 5

```

C

```

4  X(M3) = X(M3)+H6*XDOT(M3)-Q(M3)/3.0D0
   RKLCE2 = 1.
   IF (ICCNT.EC.NEQ) RKLCE2=2.
      GC TO 6

```

C

```

5  X(M3) = X(M3)+A*(CT*XDOT(M3)-Q(M2))
   C(M3) = H3*A*XDOT(M3)+(1.0D0-3.0D0*A)*Q(M3)
   RKLCE2 = 1.

```

C

```

6  RETURN
   ENC

```

C

```

FUNCTION RKLDE3 (X,XDOT,NR3)
DIMENSION X(4), XDOT(4), Q(25)
DIMENSION THAOUT(3001), XDATA(3001)
REAL *8THAOUT,XDATA
REAL *8X,XDOT,T,DT,C,H1,H2,H3,H6
REAL *8ITF
COMMON T,DT,TF,THAOUT,XDATA,M3,ICCNT,NEQ,ISKIP,ITF

```

C

```

      GC TO (1,2,3,4), NR3
1  IT = DT

```

20  
30  
40  
50  
60  
70  
80  
90  
100  
110  
120  
130  
140  
150  
160  
170  
180  
190  
200  
210  
220  
230  
240  
250  
260  
270  
280  
290  
300  
310  
320  
330  
340  
350  
360  
370  
380  
390  
400  
410  
420  
430  
440  
450  
460  
470  
480  
490  
500



```

110 F2 = H1*0.500
120 F3 = H1*2.000
130 F4 = H1/6.000
140 C(M3) = 0.00
150 A = 0.500
160 GC TO 5
170
180 2 A = 0.2928932188134525
190 GC TO 5
200
210 3 A = 1.7071067811865475
220 GC TO 5
230
240 4 X(M3) = X(M3)+H6*XDOT(M3)-Q(M3)/3.00
250 RKLCE3 = 1.
260 IF (ICONT.EQ.NEQ) RKLCE3=2.
270 GC TO 6
280
290 5 X(M3) = X(M3)+A*(CT*XDOT(M3)-Q(M3))
300 C(M3) = H3*A*XDOT(M3)+(1.00-3.00*A)*Q(M3)
310 RKLCE3 = 1.
320 RETURN
330 ENC
340
350 C
360 C
370 C
380 C
390 C
400 C
410 C
420 C
430 C
440 C
450 C
460 C
470 C
480 C
490 C
500 C
510 C
520 C
530 C
540 C
550 C
560 C
570 C
580 C
590 C
600 C
610 C
620 C
630 C
640 C
650 C
660 C
670 C
680 C
690 C
700 C
710 C
720 C
730 C
740 C
750 C
760 C
770 C
780 C
790 C
800 C
810 C
820 C
830 C
840 C
850 C
860 C
870 C
880 C
890 C
900 C
910 C
920 C
930 C
940 C
950 C
960 C
970 C
980 C
990 C

```





100  
1100  
11200  
11300  
11400  
11500  
11600  
11700  
11800  
11900  
22100  
22200  
22300  
22400  
22500  
22600  
22700  
22800  
22900  
33100  
33200  
33300  
33400  
33500  
33600  
33700  
33800  
33900  
44100  
44200  
44300  
44400  
44500  
44600  
44700  
44800  
44900  
55100  
55200  
55300  
55400  
55500  
55600  
55700

```

REAL *4LABA/' A ',LABC/' D ' /
READ (5,2) TITLE
TITLE IS ON TWO CARDS AND MUST HAVE YOUR ID
AND GRAPH TITLE IN COL 1-48.

T = 0.
TSTEP = 5.0*DT
J = 0
BIGX = 0.
BIGY = 0.
SMLX = 0.
SMLY = 0.

CC 1 I=1, IOP, 5
J = J+1
XX(J) = T
YY(J) = XDATA(I)
W(J) = THAOUT(I)
XC = YY(J)
TF = W(J)
YMAX = AMAX1(XD, TH)
YMIN = AMIN1(XD, TH)
XMAX = AMAX1(BIGX, X)
IF (BIGX.LT.X) BIGX=X
IF (BIGY.LT.YMAX) BIGY=YMAX
IF (SMLY.GT.YMIN) SMLY=YMIN
T = T+TSTEP
1 CONTINUE

TX(1) = 0.
TX(2) = 0.
TX(3) = SMLX
TX(4) = BIGX
TY(1) = BIGY
TY(2) = SMLY
TY(3) = 0.
TY(4) = 0.

PLOT SYSTEM RESPONSE
SYMBOL 'A' IS ACTUAL RESPONSE, SYMBL 'D' IS DESIRED DATA RESPONSE

CALL CRAW (4, TX, TY, 1, 1, LABC, TITLE, C, 0, 0, 0, 0, 8, 8, 0, L)
CALL CRAW (NPPLT, XX, WW, 2, 0, LABA, TITLE, 0, 0, 0, 0, 8, 8, 0, L)

FLCT DESIRED RESPONSE

```

```

C      CALL DRAW (NPPLT,XX,YY,3,0,LABD,TITLE,0,0,0,0,0,0,8,8,0,L)
C      IF (L.NE.0) WRITE (6,3) L
C      RETURN
C      3 FCRMAT (6A8)
C      FCRMAT (//,1 GRAPH NOT COMPLETED. OUTPUT CCCC = ',12)
C      END
C      SLROUTINE PPLT (XCATA,THAOUT,DT,NPPLT,ICP)
C      THIS ROUTINE PRODUCES THE PRINTER PLOTS.
C      DIMENSION XX(900), YY(900), WW(900)
C      DIMENSION TX(4), TY(4)
C      REAL *8XCATA(3001),THAOUT(3001),DT
C      CHANGE VARIABLES TO REAL*4 AND SET UP PLOT POINTS.
C      CLEAR REGISTERS AND SET AXIS. REG. PROBABLY CC NOT HAVE TO CLEAR A
C      CHECK ON LATER.....
C      CC 1 I=1,500
C      XX(I) = 0.
C      YY(I) = 0.
C      1 WW(I) = 0.
C      T = 0.
C      TSTEP = 5.0*DT
C      J = 0
C      BIGX = 0.
C      BIGY = 0.
C      SMLX = 0.
C      SMLY = 0.
C      DO 2 I=1,1DP,5
C      J = J+1
C      XX(J) = T
C      YY(J) = XDATA(I)
C      WW(J) = THAOUT(I)
C      X = T
C      XC = YY(J)
C      TH = WW(J)
C      YMAX = AMAX1(XD,TH)
C      YMIN = AMIN1(XD,TH)
C      XMAX = AMAX1(BIGX,X)
C      IF (BIGX.LT.X) BIGX=X

```

```

400 IF (BIGY.LT.YMAX) BIGY=YMAX
410 IF (SMLY.GT.YMIN) SMLY=YMIN
420 I = I+1 STEP
430 2 CONTINUE
440 TX(1) = 0.
450 TX(2) = 0. SMLX
460 TX(3) = 0. SMLX
470 TX(4) = 0. SMLX
480 TY(1) = 0. BIGY
490 TY(2) = 0. BIGY
500 TY(3) = 0. SMLY
510 TY(4) = 0. SMLY
520 WRITE (6,3) BIGX,BIGY,SMLY
530
540 PLCT SYSTEM RESPONSE. "*" IS DESIRED RESPONSE. "+" IS ACTUAL
550 RESPONSE. "*" ONLY INDICATE COINCIDENCE OF CURVES.
560
570 CALL FLCIP (TX,TY,4,1)
580 CALL FLCIP (XX,WW,NPPLT,2)
590 CALL FLCIP (XX,YY,NPPLT,3)
600 WRITE (6,4)
610 IF (IDP.EQ.4500) WRITE (6,5)
620 RETURN
630
640 FCRMAT (2X,'BIGX= ',E15.7,2X,'BIGY= ',E15.7,2X,'SMLY= ',E15.7)
650 FCRMAT (//,2X,'SYSTEM RESPONSE FOR PROBLEM -----')
660 FCRMAT (//,2X,'STEP AT 500 GRAPH FCINTS')
670 EN
680
690 .....
700 SLROUTINE BOXPLX (CATEGORY F0)
710
720 PURPOSE
730
740 BOXPLX IS A SUBROUTINE USED TO SOLVE THE PROBLEM OF LOCATING
750 A MINIMUM (OR MAXIMUM) OF AN ARBITRARY OBJECTIVE FUNCTION BY
760 SUBJECT TO ARBITRARY EXPLICIT AND/OR IMPLICIT CONSTRAINTS.
770 THE COMPLEX UPPER AND LOWER BOUNDS ON THE FUNCTIONAL VARIATION
780 DEFINED AS CONSTRAINTS MAY BE PROGRAMMED TO EVALUATE THE OBJECTIVE
790 IMPLICITLY AND IMPLICITLY (SEE EXAMPLE PROGRAMMING, WHERE VALUES
800 SUPPLIED BY THE USER TO PERFORM PROGRAMMING, WHERE VALUES
810 OF THE INDEPENDENT VARIABLES ARE RESTRICTED TO INTEGERS.
820
830 USAGE
840
850 .....
860 BXPX0010
870 BXPX0020
880 BXPX0030
890 BXPX0040
900 BXPX0050
910 BXPX0060
920 BXPX0070
930 BXPX0080
940 BXPX0090
950 BXPX0100
960 BXPX0110
970 BXPX0120
980 BXPX0130
990 BXPX0140
1000 BXPX0150
1010 BXPX0160
1020 BXPX0170
1030 BXPX0180
1040 BXPX0190

```

BXPX0200  
 BXPX0210  
 BXPX0220  
 BXPX0230  
 BXPX0240  
 BXPX0250  
 BXPX0260  
 BXPX0270  
 BXPX0280  
 BXPX0290  
 BXPX0300  
 BXPX0310  
 BXPX0320  
 BXPX0330  
 BXPX0340  
 BXPX0350  
 BXPX0360  
 BXPX0370  
 BXPX0380  
 BXPX0390  
 BXPX0400  
 BXPX0410  
 BXPX0420  
 BXPX0430  
 BXPX0440  
 BXPX0450  
 BXPX0460  
 BXPX0470  
 BXPX0480  
 BXPX0490  
 BXPX0500  
 BXPX0510  
 BXPX0520  
 BXPX0530  
 BXPX0540  
 BXPX0550  
 BXPX0560  
 BXPX0570  
 BXPX0580  
 BXPX0590  
 BXPX0600  
 BXPX0610  
 BXPX0620  
 BXPX0630  
 BXPX0640  
 BXPX0650  
 BXPX0660  
 BXPX0670

CALL BOXPLX (NV,NAV,NPR,NTA,R,XS,IP,XU,XL,YMN,IER)

DESCRIPTION OF PARAMETERS

NV AN INTEGER INPUT DEFINING THE NUMBER OF INDEPENDENT  
 VARIABLES OF THE OBJECTIVE FUNCTION TO BE MINIMIZED. IS  
 NOTE: MAXIMUM NV + NAV IS PRESENTLY 50. PUNCH A SOURCE  
 25. IF THESE LIMITS MUST BE EXCEEDED, THE DIMENSION  
 DECK IN THE USUAL MANNER, AND CHANGE THE DIMENSION  
 STATEMENTS.  
  
 NAV AN INTEGER INPUT DEFINING THE NUMBER OF AUXILIARY VAR-  
 IABLES THE USER WISHES TO DEFINE FOR HIS OWN CONVENIENCE.  
 TYPICALLY HE MAY WISH TO DEFINE THE VALUE OF EACH  
 CONSTRAINT FUNCTION AS AN AUXILIARY VARIABLE. IF THIS  
 IS DONE, THE OPTIONAL OUTPUT OF BCKFLX CAN BE  
 USED TO OBSERVE THE VALUES OF THE CONSTRAINTS AS THE  
 SOLUTION PROGRESSES. AUXILIARY VARIABLES IF USED,  
 SHOULD BE EVALUATED IN FUNCTION KE (DEFINED BELOW).  
 NAV MAY BE ZERO.  
  
 NPR INPUT INTEGER CONTROLLING THE FREQUENCY OF OUTPUT DESIRED  
 FOR DIAGNOSTIC PURPOSES. IF NPR = 0, NO OUTPUT WILL BE  
 PRODUCED BY BOXPLX. OTHERWISE, THE CURRENT COMPLEX AFTER  
 K = 2\*NV VERTICES AND THEIR CENTROIDS WILL BE OUTPUT AFTER  
 EACH NPR PERMISSIBLE TRIALS. THE NUMBER OF TOTAL TRIALS,  
 AND NUMBER OF FEASIBLE TRIALS, NUMBER OF FUNCTION EVALUATIONS,  
 AND NUMBER OF IMPLICIT CONSTRAINT EVALUATIONS ARE IN-  
 CLUDED IN THE OUTPUT.  
 ADDITIONALLY, (WHEN NPR = GT. 0) THE SAME INFORMATION  
 WILL BE OUTPUT:  
 1) IF THE INITIAL POINT IS NOT FEASIBLE  
 2) AFTER THE FIRST COMPLETE COMPLEX IS GENERATED  
 3) IF A FEASIBLE VERTEX CANNOT BE FOUND AT SOME TRIAL,  
 4) IF THE OBJECTIVE VALUE OF A VERTEX CANNOT BE MADE  
 NO-LARGER-WORST.  
 5) IF THE LIMIT ON TRIALS (NTA) IS REACHED AND  
 6) WHEN THE OBJECTIVE FUNCTION HAS BEEN UNCHANGED FOR  
 2\*NV TRIALS, INDICATING A LOCAL MINIMUM HAS BEEN  
 FOUND.  
  
 IF THE USER WISHES TO TRACE THE PROGRESS OF A SOLUTION,  
 A CHOICE OF NPR = 25, 50 OR 100 IS RECOMMENDED.  
  
 NTA INTEGER INPUT OF LIMIT ON THE NUMBER OF TRIALS ALLOWED



IN THE CALCULATION. IF THE USER INPUTS NTA .LE. 0, A  
 DEFAULT VALUE OF 2000 IS USED. WHEN THIS LIMIT IS REACHED  
 CONTROL RETURNS TO THE CALLING PROGRAM WITH THE BEST  
 ATTAINED OBJECTIVE FUNCTION VALUE IN YMN, AND THE BEST  
 ATTAINED SOLUTION POINT IN XS.

R A REAL NUMBER INPUT TO DEFINE THE FIRST RANDCM NUMBER  
 USED IN DEVELOPING THE INITIAL COMPLEX OF 2\*NV VERTICES.  
 (0. .GT. R .LT. 1.) IF R IS NOT WITHIN THESE BOUNDS,  
 IT WILL BE REPLACED BY 1./3. .

XS INPUT REAL ARRAY DIMENSIONED AT LEAST NV+NAV. THE FIRST  
 NV MUST CONTAIN A FEASIBLE ORIGIN FOR STARTING THE CAL-  
 CULATION. THE LAST NAV NEED NOT BE INITIALIZED. LPCN  
 RETURN FROM BOXPLX, THE FIRST NV ELEMENTS OF THE ARRAY  
 CONTAIN THE COORDINATES OF THE MINIMUM OBJECTIVE FUNCTION,  
 AND THE REMAINING NAV (NAV .GE. 0) CONTAIN THE VALUES OF  
 THE CORRESPONDING AUXILIARY VARIABLES.

IP INTEGER INPUT FOR OPTIONAL INTEGER PROGRAMMING. IF IP=1,  
 THE VALUES OF THE INDEPENDENT VARIABLES WILL BE REPLACED  
 WITH INTEGER VALUES (STILL STORED AS REAL\*4).

XU A REAL ARRAY DIMENSIONED AT LEAST NV INPUTTING THE UPPER  
 BOUND ON EACH INDEPENDENT VARIABLE, (EACH EXPLICIT CON-  
 STRAINT). INPUT VALUES ARE SLIGHTLY ALTERED BY BOXPLX.

XL A REAL ARRAY DIMENSIONED AT LEAST NV INPUTTING THE LOWER  
 BOUND ON EACH INDEPENDENT VARIABLE. (EACH EXPLICIT CON-  
 STRAINT). NOTE: FOR BOTH XU AND XL CHOICE REASONABLE  
 VALUES IF NONE ARE GIVEN, NOT VALUES WHICH ARE MAGNITUDES  
 ABOVE OR BELOW THE EXPECTED SOLUTION. INPUT VALUES ARE  
 SLIGHTLY ALTERED BY BOXPLX.

YMN THIS OUTPUT IS THE VALUE (REAL\*4) OF THE OBJECTIVE FUNC-  
 TION, CORRESPONDING TO THE SOLUTION POINT OUTPUT IN XS.

IER INTEGER ERROR RETURN. TO BE INTERRUPTED LPCN RETURN  
 FROM BOXPLX. IER WILL BE ONE OF THE FOLLOWING:

==1 CANNOT FIND FEASIBLE VERTEX OR FEASIBLE CENTRIC  
 AT THE START OR A RANGED START (SEE METHFC, BELCW).  
 =0 FUNCTION VALUES UNCHANGED FOR N TRIALS. (WHERE  
 N=6\*NV+10) THIS IS THE VERTEX.  
 =1 CANNOT DEVELOP FEASIBLE VERTEX.  
 =2 CANNOT DEVELOP A NC-LONGER (NTA EXCEEDED)  
 =3 LIMIT ON TRIALS REACHED. RETURNED IN ANY OF THE

NOTE:  
 INVALID RESULTS MAY BE RETURNED IN ANY OF THE

[illegible]



[illegible]



BXFX22600  
BXFX22610  
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BXFX23070

SUBROUTINES AND FUNCTIONS REQUIRED

SUBROUTINE 'BOUN' AND FUNCTION 'FBV' ARE INTEGRAL PARTS OF THE BOXPLX PACKAGE.

TWO FUNCTIONS MUST BE SUPPLIED BY THE USER. THE FIRST, KE(X), IS USED TO EVALUATE THE IMPLICIT CONSTRAINTS. SET KE=0 AT THE BEGINNING OF THE FUNCTION, THEN EVALUATE THE IMPLICIT CONSTRAINTS. IN THE EXAMPLE ABOVE, THE FIRST CONSTRAINT, X(3), MUST BE WITHIN THE RANGE (0.0, 6.0). THE SECOND CONSTRAINT, X(4), MUST BE GE. 0.0. IF EITHERED TO STATEMENT 1, NOT WITHIN THESE BOUNDS, CONTROL IS RETURNED TO ECXPLX. AND KE IS SET TO "1" AND CONTROL IS RETURNED TO ECXPLX.

THE SECOND FUNCTION THE USER MUST PROVIDE EVALUATES THE OBJECTIVE FUNCTION. IT IS CALLED FE(X) AS SPEC'N IN THE EXAMPLE ABOVE, AND FE MUST BE SET TO THE VALUE OF THE OBJECTIVE FUNCTION CORRESPONDING TO CURRENT VALUES OF THE NV INDEPENDENT VARIABLES IN ARRAY 'X'.

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EVERIDGE G., AND SCHECHTER R., "OPTIMIZATION: THEORY AND PRACTICE", MCGRAW-HILL, 1970.

PROGRAMMER

R. R. HILLEARY 1/1966.  
REVISED FOR SYSTEM 360 4/1967  
CORRECTED 1/1969  
REVISED/EXTENDED BY L. NOLAN/R. HILLEARY 2/1975

.....

SUBROUTINE BOXPLX (NV, NAV, NPR, NTZ, RZ, XS, IF, EU, BL, YMN, IER)  
DIMENSION V(50,50), FUN(50), SUM(25), CEN(25), XS(NV), EU(NV), BL(NV)

KV = 5  
EF = 1.0E-6



107

```

C      NUMEER OF CONSECUTIVE TRIALS WITH UNCHANGED FE TO TERMINATE.
C      NCT = NLIM+NV
C      ALPHA = 1.3
C      FK = K
C      FKM = FK-1.
C      BETA = ALPHA+1.
C
C      INSURE SEED OF RANDCM NUMBER GENERATOR IS CCC.
C      IQR = R*1.E7
C      IF (MOD(IQR,2).EQ.0) IQR=IQR+101
C
C      SET UP INITIAL VERTICES
C      FUN(1) = FE(V(1,1))
C      YMN = FUN(1)
C      FI = 1.
C      FUNGLD = FUN(1)
C
C      DO 15 I=2,K
C      FJ = FI+1.
C      LIMIT = 0
C      7 LIMIT = LIMIT+1
C
C      ENC CALCULATION IF FEASIBLE CENTROIC CANNOT BE FOUND.
C      IF (LIMIT.GE.NLIM) GO TO 11
C
C      DO 8 J=1,NV
C
C      RANDCM NUMBER GENERATOR (RANCU)
C      IQR = IQR*.65535
C      IF (IQR.LT.0) IQR = IQR+2147483647+1
C      RCX = IQR
C      RCX = RCX*.4656613E-9
C      V(J,I) = BL(J)+RQX*(BL(J)-BL(J))
C      IF (IP.EQ.1) V(J,I)=AINT(V(J,I)+.5)
C      8 CCNTINCE
C
C      DO 10 L=1,NLIM
C      NCE = NCE+1
C      IF (KE(V(1,I)).EQ.0) GO TO 13
C
C      DO 9 J=1,NV
C      VT = .5*(V(J,I)+CEN(J))
C      IF (IP.EQ.1) VT = AINT(VT+.5)
C      V(J,I) = VT
C      9 CCNTINCE
C      10 CCNTINCE

```

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BXFX3560
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BXFX3990
BXFX4000
BXFX4010
BXFX4020
BXFX4030

```

```

C      11 IF (NPR.LE.0) GO TO 12
        WRITE (6,51) I
        CALL BOUT (NT,NPT,NFE,NCE,NV,NVT,V,I,FUN,CEN,I)
C      12 IER = -1
        GO TO 4E
C      13 CC 14 J=1,NV
        SUM(J) = SUM(J)+V(J,I)
C      14 CEN(J) = SUM(J)/FI
C      TRY TO ASSURE FEASIBLE CENTROID FOR STARTING.
        NCE = NCE+1
        IF (KE(CEN).NE.0) GO TO 7
        NFE = NFE+1
        FUN(I) = FE(V(1,I))
C      15 CCNTINUE
C      END OF LOOP SETTING OF INITIAL COMPLEX.
        IF (NPR.LE.0) GO TO 17
        CALL BOUT (NT,NPT,NFE,NCE,NV,NVT,V,K,FUN,CEN,0)
C      FIND THE WORST VERTEX, THE 'J'TH.
        J = 1
C      CC 16 I=2,K
        IF (FUN(J).GE.FUN(I)) GC TO 16
        J = I
C      16 CCNTINUE
C      BASIC LOOP. ELIMINATE EACH WORST VERTEX IN TURN. IT MUST BECCME
C      NO LONGER WORST, NOT MERELY IMPROVED. FIND NEXT-TO-WORST VERTEX,
C      THE 'JN'TH ONE.
C      17 JN = 1
        IF (J.EC.1) JN = 2
C      CC 18 I=1,K
        IF (I.EC.J) GC TO 18
        IF (FUN(JN).GE.FUN(I)) GO TO 18
        JN = I
C      18 CCNTINUE
C      LIMIT = NUMBER OF MOVES DURING THIS TRIAL TOWARD THE CENTROID
C      CUE TO FUNCTION VALUE.
        LIMIT = 1
C      COMPLETE CENTROID AND OVER REFLECT WORST VERTEX.

```

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```

C 15 I=1,NV
C     VT = V(I,J)
C     SUM(I) = SUM(I)-VT
C     CEN(I) = SUM(I)/FKM
C     VT = BETA*CEN(I)-ALPHA*VT
C     IF (IP.EQ.1) VT = AINT(VT+.5)
C
C     INSURE THE EXPLICIT CCNSTRANTS ARE CBSERVED.
C 15 V(I,J) = AMAX1(AMINI(VT,BU(I)),BL(I))
C
C     NT = NT+1
C
C     CHECK FOR IMPLICIT CCNSTRANT VIOLATION.
C
C 20 CC 25 N=1,NLIM
C     NCE = NCE+1
C     IF (KE(V(1,J)).EQ.0) GO TO 26
C
C     EVERY .KV. TH TIME, CVER-REFLECT THE OFFENDING VERTEX THROUGH THE
C     BEST VERTEX.
C     IF (MOD(N,KV).NE.0) GO TO 22
C     CALL FBV (K,FUN,M)
C
C 21 I=1,NV
C     VT = BETA*V(I,M)-ALPHA*V(I,J)
C     IF (IP.EQ.1) VT = AINT(VT+.5)
C     21 V(I,J) = AMAX1(AMINI(VT,BU(I)),BL(I))
C
C     GO TO 24
C
C     CCNSTRANT VIOLATION:  MCVE NEW POINT TOWARC CENTROIC.
C
C 22 CC 23 I=1,NV
C     VT = .5*(CEN(I)+V(I,J))
C     IF (IP.EQ.1) VT = AINT(VT+.5)
C     V(I,J) = VT
C 23 CCNTINUE
C
C 24 NT = NT+1
C 25 CCNTINUE
C
C     IER = 1
C
C     CANNOT GET FEASIBLE VERTEX BY MOVING TOWARD CENTROIC,
C     TRY CVER-REFLECTING THRU THE BEST VERTEX.
C     IF (NPR.LE.0) GO TO 42
C     WRITE (6,52) NT,J
C     CALL BGLT (NT,NPT,NFE,NCE,NV,NVT,V,K,FUN,CEN,J)

```



```

GC TO 42
FEASIBLE VERTEX FOUND, EVALUATE THE OBJECTIVE FUNCTION.
26 NFE=NFE+1
   FLNTRY = FE(V(1,J))

TEST TO SEE IF FUNCTION VALUE HAS NOT CHANGED.
   AFC = ABS(FUNTRY-FUNCOLD)
   AMX = AMAX1(ABS(EP*FUNCOLD),EP)

ACTIVATE THE FOLLOWING TWO STATEMENTS FOR DIAGNOSTIC PURPOSES ONLY.
   WRITE(6,55) J,AFC,AMX,FUNTRY,FUNCOLD,FUN(J),FUN(JN),NTFS,K
55 FORMAT(1X,I3,6E15.7,2F5)
   IF (AFC.GT.AMX) GC TO 27
   NTFS = NTFS+1
   IF (NTFS.LT.NCT) GC TO 28
   IF (NCT.EQ.NCT) GC TO 42
   IF (NPP.LE.0) GC TO 42
   WRITE(6,53) K
GC TO 42
27 NTFS = 0

IS THE NEW VERTEX NO LONGER WORST?
28 IF (FUNTRY.LT.FUN(JN)) GO TO 34

TRIAL VERTEX IS STILL WORST: ADJUST TOWARD CENTROID THROUGH THE
EVERY KTH TIME, OVER-REFLECT THE OFFENDING VERTEX
BEST VERTEX.
   LIMIT = LIMIT+1
   IF (MCE(LIMIT,KV).NE.0) GO TO 30
   CALL FBV(K,FUN,M)

CC 29 I=1,NV
   VT = BETA*V(I,M)-ALPHA*V(I,J)
   IF (IP.EQ.1) VT = AINT(VT+.5)
29 V(I,J) = AMAX1(AMIN1(VT,BU(I)),BL(I))

GC TO 32

CC 30 I=1,NV
   VT = .5*(CEN(I)+V(I,J))
   IF (IP.EQ.1) VT = AINT(VT+.5)
   V(I,J) = VT
31 CONTINUE

CC 32 IF (LIMIT.LT.NLIMIT) GC TO 33

CANNOT MAKE THE JTH VERTEX NO LONGER WORST BY DISPLACING TOWARD

```

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BXPX5480
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BXPX5940
BXPX5950

```

```

C THE CENTROID OR BY OVER-REFLECTING THRU THE BEST VERTEX.
  IER = 2
  IF (NPR.GT.0) WRITE (6,52) NT,J
  GO TO 42
33 NT = NT+1
  GO TO 20

C
C SUCCESS: WE HAVE A REPLACEMENT FOR VERTEX J.
34 FUN(J) = FUNTRY
  FUNCLD = FUNTRY
  NPT = NPT+1

C
C EVERY 100TH PERMISSIBLE TRIAL, RECCMPUTE CENTROID SUMMATION TC
  IVCIC CREEPING ERROR.
  IF (MCC(NPT,100).NE.0) GO TO 37

  CC 36 I=1,NV
  SUM(I) = 0.

  CC 35 N=1,K
  SUM(I) = SUM(I)+V(I,N)

  CC 34 CEN(I) = SUM(I)/FK
  CC 33 CCNTINUE

  CC 32 LC = 0
  GO TO 39

  CC 31 CC 38 I=1,NV
  SUM(I) = SUM(I)+V(I,J)

  CC 30 LC = J

  CC 29 IF (NPR.LE.0) GO TO 40
  IF (MCC(NPT,NPR).NE.0) GO TO 40

  CC 28 CALL BCUT (NT,NPT,NFE,NCE,NV,NVT,V,K,FUN,CEN,LC)

  CC 27 HAS THE MAX. NUMBER OF TRIALS BEEN REACHED WITHOUT CONVERGENCE?
  IF ACT, GO TO NEW TRIAL.
  40 IF (NT.GE.NTA) GO TO 41

  CC 26 NEXT-TC-WCRST VERTEX NOW BECOMES WCRST.
  J = JN
  CC TC 17
  41 IEF = 3
  IF (NPR.GT.0) WRITE (6,54)

C

```

```

C COLLECTOR POINT FOR ALL ENDINGS.
C 1) CANNOT DEVELOP FEASIBLE VERTEX.
C 2) CANNOT DEVELOP A NO-LONGER-WORST VERTEX.
C 3) FUNCTION VALUE UNCHANGED FOR K TRIALS.
C 4) LIMIT ON TRIALS REACHED.
C 5) CANNOT FIND FEASIBLE VERTEX AT START.
C 42 CONTINUE
C
C FIND BEST VERTEX.
C CALL FBV (K,FUN,M)
C IF (IER.GE.3) GO TO 44
C
C RESTART IF THIS SOLUTION IS SIGNIFICANTLY BETTER THAN THE PREVIOUS,
C CR IF THIS IS THE FIRST TRY.
C IF (NPR.LE.0) GO TO 43
C WRITE (6,55) (M,YMN,FUN(M))
C 43 IF (FUN(M).GE.YMN) GO TO 47
C IF (ABS(FUN(M)-YMN).LE.AMAX1(EP,EP*YMN)) GO TO 47
C
C GIVE IT ANOTHER TRY UNLESS LIMIT ON TRIALS REACHED.
C 44 YMN = FUN(M)
C FUN(1) = FUN(M)
C
C 45 I=1,NV
C CEN(I) = V(I,M)
C SUM(I) = V(I,M)
C 45 V(I,1) = V(I,M)
C
C 46 I=1,NVT
C XS(I) = V(I,M)
C
C IF (IER.LT.3) GO TO 6
C 47 IF (NPR.LE.0) GO TO 48
C CALL BCLT (NT,NPT,NFE,NCE,NV,NVT,V,K,FUN,V(1,M),-1)
C WRITE (6,56) FUN(M)
C RETURN
C
C 49 FCRMAT (50) INDEX AND DIRECTION OF OUTLYING VARIABLE AT START IS
C 50 FCRMAT (50) IMPLICIT CONSTRAINT VIOLATED AT START. LEAD ENC.
C 51 FCRMAT (50) CANNOT FIND FEASIBLE, I4, TH VERTEX OR CENTROID AT START
C 51 FCRMAT (50)
C 52 FCRMAT (10) AT TRIAL I4, 54H CANNOT FIND FEASIBLE VERTEX WHICH IS
C 52 FCRMAT (10) WORST, I4, 15X, RESTART FROM BEST VERTEX.
C 53 FCRMAT (40) OF FUNCTION HAS BEEN ALMOST UNCHANGED FOR I5, 7H TRIALS
C 54 FCRMAT (27) OF LIMIT ON TRIALS EXCEEDED.
C 55 FCRMAT (50) BEST VERTEX IS NO., I3, CLD MIN WAS ,E15.7,
C 55 FCRMAT (50) MIN IS ,E15.7
C 56 FCRMAT (50) MIN OBJECTIVE FUNCTION IS ,E15.7

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```

IER = 1
IER = 2
IER = 0
IER = 3
IER = -1

```

```

C
ENCL
SLEROUTINE FBV (K,FUN,M)
DIMENSION FUN(50)
M = 1
C
CC 1 I=2,K
IF (FUN(M).LE.FUN(I)) GC TO 1
M = I
1 CCNTINUE
C
RETURN
ENCL
SLEROUTINE BOUT (NT,NPT,NFE,NCE,NV,NVT,V,K, FN,C, IK)
DIMENSION V(50,50), FN(50), C(25)
WRITE (6,4) NT,NPT,NFE,NCE
C
CC 1 I=1,K
WRITE (6,5) FN(I),(V(J,I),J=1,NV)
IF (NVT.LE.NV) GO TO 1
NVF = NV+1
WRITE (6,6) (V(J,I),J=NVP,NVT)
1 CCNTINUE
C
IF (IK.NE.0) GO TO 2
C
WRITE (6,7) (C(I),I=1,NV)
RETURN
2 IF (IK.GE.0) GO TO 3
WRITE (6,8) (C(I),I=1,NV)
RETURN
3 WRITE (6,9) IK,(C(I),I=1,NV)
RETURN
C
4 FCRMAT (,ONO, TOTAL TRIALS = ,I5,4X,NO, FEASIBLE TRIALS = ,EVALUATION
1 I5,4X,NO, FUNCTION EVALUATIONS = ,I5,4X,AC,CONSTRAINT EVALUATION
2 CNS = ,I5,NO, FUNCTION VALUE',6X,INDEPENDENT VARIABLES/DEPENDENT
3 ENT OR IMPLICIT CONSTRAINTS')
5 FCRMAT (1H,E18.7,2X,7E14.7/(21X,7E14.7))
6 FCRMAT (21X,7E14.7)
7 FCRMAT (10F,CENTROID 11X,7E14.7/(21X,7E14.7))
8 FCRMAT (10F,CENTROID 11X,7E14.7/(21X,7E14.7))
9 FCRMAT (10F,CENTROID 11X,7E14.7/(21X,7E14.7))
ENC
C
/* CARC GOES HERE
//GC.SYSIN CC *
C
*** THE FOLLOWING CARDS ARE THE DATA CHECK FOR PRCELEM III-B.
C
*** TACT FEEDBACK COMPENSATION.

```

C	I	1	1000	1
	0.7	0.0002	0.22	
	0.0	31.628	1000.	
	-0.0			
	-0.0			
	-0.0			
	0.0			
	12=C1C2			
	22=C203			
	31=C201			
	41=C201			

10.



## LIST OF REFERENCES

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